

**MODELLING AND FORECASTING OF FLOOD EVENTS FOR DECISION
SUPPORT IN INTEGRATED WATER RESOURCES MANAGEMENT IN GUCHA-
MIGORI RIVER BASIN, KENYA**

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**A Thesis Submitted to the Graduate School in Partial Fulfillment of the Requirements
for Master of Science Degree in Soil and Water Engineering of Egerton University**

EGERTON UNIVERSITY

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DECLARATION AND RECOMMENDATION

Declaration

This thesis is my original work and it has not been wholly or in part presented for the award of a degree or diploma in any other institution known to me.


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DEDICATION

This work is dedicated to God my creator. To my dearest husband Douglas Musa Machage, and mother Cecilia Akinyi for continuous prayers, love, support, motivation, encouragement, guidance, and mentorship. To my children Laurlyn Moraa, Zacharia Machage, Morna Kwamboka, Cecilia Bwari and Tirzah Nyambeki, may this inspire you to work hard.

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ABSTRACT

Floods are devastating natural disasters frequently striking many river basins such as Gucha-Migori River Basin nearly every year. However, non-structural countermeasures have not been fully explored and implemented to reduce damage, risk, and vulnerabilities of flood events. In light of this, the main objective of the study was to model and forecast flood events in the Gucha-Migori River Basin for decision support in integrated water resource management. Modelling the response of flood events to precipitation variability using the HEC-HMS model for the period (1973-2015) was the first activity conducted. Then a relationship between flood magnitude and frequency was developed using probability distribution model. Coefficient of Determination (R^2), Goodness of Fit test, and Best-Fit Distribution Curve guided selection of the suitable distribution model. Finally, flood events and their respective annual exceedance probabilities were forecasted using Artificial Neural Networks (ANNs) and the Gumbel distribution model for the period (2015-2052). From the results, independent flood events were detected for the years 1969, 1971, 1974, 1977, 1969, 1981, 1982, 1983, 1985, 1990, 1996, 2004, 2006, 2007, 2010, 2011, and 2013. The R^2 and Nash values for HEC-HMS model calibration and validation of daily river discharge at sub-basin 1 were 0.52 and 0.36, and, 0.42 and 0.31 respectively. The correlation coefficients between daily precipitations for JFM, AMJ, JAS, and OND, and the corresponding river discharges had a significant positive correlation at the significant level of 0.05. It was revealed that the probability of a flood event of a magnitude equal to or exceeding the lowest ($240.8 \text{ m}^3/\text{s}$) and the highest ($423.90 \text{ m}^3/\text{s}$) occurring for a particular were 0.98 and 0.02 respectively. Considering the predictions from Gumbel, Log P3, Log N, and Normal models, for the return periods 1.05 and 200 years, the flood magnitude estimated for G-M River Basin would be 221.38 and 466.65, 233 and 478, 178.19 and 367.38, and 209 and $402 \text{ m}^3/\text{s}$. Gumbel distribution curve was selected to be the best fit for the Gucha-Migori River Basin. Using the comparative analysis, the network topology of 1-20-1 was adopted as the best NAR model for forecasting because of its minimum values of R for training ($9.20\text{e-}1$), validation ($9.27\text{e-}1$), and testing ($9.15\text{e-}1$). The maximum forecasted flood magnitudes were 336, 391, 433, 299, 389, 502, and 483 m^3/s for the periods 2014–2018, 2019–2023, 2024–2028, 2029–2033, 2034–2038, 2039–2043, and 2048–2052, respectively. Their respective annual non-exceedance probabilities from the Gumbel's curve and derived equation were 84.6, 96, 98, 64, 96, 99.6, and 99 %. The information from the research offers prerequisite flood response plans and provides early flood detection and forecasting for planning for the management of flood risks and for preparedness in the Gucha-Migori River Basin.

TABLE OF CONTENT

DECLARATION AND RECOMMENDATION	ii
COPYRIGHT	iii
DEDICATION	iv
ACKNOWLEDGEMENTS	v
ABSTRACT.....	vi
LIST OF FIGURES	xi
LIST OF SYMBOLS.....	xiii
LIST OF ABBREVIATIONS AND ACRONYMS	xiv
CHAPTER ONE	1
INTRODUCTION.....	1
1.1 Background Information	1
1.2 Statement of the Problem	2
1.3 Objectives.....	3
1.3.1 Broad Objective	3
1.3.2 Specific Objectives	3
1.4 Research Questions.....	4
1.5 Justification	4
1.6 Scope and Limitations of the Study.....	6
1.7 Definition of terms.....	6
CHAPTER TWO	8
LITERATURE REVIEW	8
2.1 Flood	8
2.2 Response of Flood Events to Precipitation Variability.....	9
2.2.1 Hydrologic Modelling	11
2.2.2 Hydrologic Engineering Centre - Hydrologic Modeling System (HEC-HMS).....	12
2.2.3 Hydrologic Engineering Centre -Geospatial Hydrologic Modeling Extension	15
2.2.4 HEC-HMS Model Calibration and Validation	15
2.2.5 Hydrologic Model Performance Assessment	16
2.3 Flood Frequency and Probability Distribution Models	18
2.3.1 Flood Frequency	19
2.3.2 Probability Distribution Functions (PDFs)	19
2.4 Forecasting of Flood Events.....	22
2.4.1 Artificial Neural Network	22

2.4.2 Coupling ANN with the Probability Distribution Models	24
CHAPTER THREE	26
MATERIALS AND METHODS	26
3.1 The Study Area.....	26
3.1.1 Spatial Data Collection	27
3.1.2 Climate Variables, Hydrologic, and Field Data Acquisition	27
3.2 Modelling Response of River Discharge to Precipitation Variability	28
3.2.1 Precipitation Variability	28
3.2.2 Modelling of River Discharge Using HEC-HMS.....	28
3.2.3 Processing of Digital Elevation Model Data.....	28
3.2.4 Processing of Soil Data and Land Use - Land Cover Maps Datasets.....	29
3.2.5 Preparation of Hydrologic and Meteorological Datasets	30
3.2.6 HEC-HMS Set-up and Run	30
3.2.7 HEC-HMS Model Sensitivity Analysis	33
3.2.8 HEC-HMS Model Calibration and Validation	33
3.2.9 HEC-HMS Model Performance Assessment	34
3.2.10 Discharge Hydrometric Indices and Precipitation Variability Correlation.....	34
3.3 Developing the Relationship between Flood Magnitude and Frequency	37
3.3.1 Flood Frequency Analysis	37
3.3.2 Modelling Using Probability Distribution Models	38
3.3.3 Selection of Probability Distribution Model	39
3.3.4 Coefficient of Determination (R ²).....	39
3.3.5 Goodness of Fit (GoF) Test.....	40
3.3.6 Anderson-Darling (AD) Test.....	40
3.3.7 Kolmogorov-Smirnov Test.....	41
3.3.8 Cramer-Von Mises Test	41
3.3.9 Best-Fit Distribution Curve	41
3.3.10 Estimation of Flood Magnitudes and Probability of Exceedance	42
3.4 Forecasting of Flood Events and their Respective AET	44
CHAPTER FOUR.....	46
RESULTS AND DISCUSSION	46
4.1 Modelling Response of River Discharge to Precipitation Variability	46
4.1.1 Precipitation Variability	46
4.1.2 Calibration and Validation of the HEC-HMS Model	50

4.1.3 Correlation between River Discharge and Precipitation Variability	54
4.2 Correlation of Flood Magnitude and Frequency using PDFs	57
4.2.1 Flood Frequency Analysis.....	57
4.2.2 Performance of Probability Distribution Models	58
4.2.3 Suitable Probability Distribution Curve Based on R2	61
4.2.4 GoF Statistics-Based Assessment for Suitable PDC	62
4.2.6 Best-Fit Distribution Curve	63
4.2.7 Probability Distribution Curve for Gucha-Migori River Basin.....	64
4.3 Forecasting of the Flood Magnitude and Percent Annual Exceedance	65
4.3.1 Nonlinear Autoregressive Models Performance.....	65
4.3.2 Best NAR Performance Indicators	67
4.3.3 Time Series of Observed and Predicted Future Flood Events.....	70
CHAPTER FIVE.....	72
CONCLUSIONS AND RECOMMENDATIONS.....	72
5.1 Conclusions	72
5.2 Recommendations.....	73
REFERENCES.....	74
APPENDICES.....	91
Appendix A: Tables.....	91
Appendix B: Figures.....	93
Appendix C: Research License	101
Appendix D: Publication	102

LIST OF TABLES

Table 2.1: General performance ratings for recommended statistics.....	17
Table 2.2: The parameters and PD functions	20
Table 3.1: Satellite remote sensing and Geospatial data products.....	27
Table 4.1: Initial Parameters from HEC-GeoHMS Used in the HEC-HMS Model.....	50
Table 4.2: Log Pearson 3 Parameters and Estimated Flood Magnitudes	59
Table 4.3: Log Normal Parameters and Estimated Flood Magnitudes	59
Table 4.4: Gumbel's Parameters and Estimated Flood Magnitudes	60
Table 4.5: Comparison of Goodness-of-fit Statistics.....	62
Table 4.6: Best fit distribution model selection based on AIC.....	63
Table 4.7: Nonlinear Autoregressive Models Performance	66

LIST OF FIGURES

Figure 2.1: Flood Hydrograph	8
Figure 2.2: Schematic Diagram of the Rainfall-Runoff Process in HEC-HMS	14
Figure 2.3: Overview of HEC-GeoHMS Program	15
Figure 2.4: Flowchart of the procedure for flood magnitude estimation using the PDFs	21
Figure 2.5: A typical Artificial Neurons Architecture	23
Figure 2.6: Types of Artificial Neural Network activation (transfer) functions	24
Figure 3.1: Gucha-Migori River Basin	26
Figure 3.2: The Flow chart showing Modelling of Flood Routing by HEC-HMS.....	31
Figure 3.3: General schematic framework for flood magnitude forecasting.....	43
Figure 3.4: The NAR neural network for forecasting flood magnitudes	44
Figure 4.1: Precipitation Anomaly for the Months of January, February, and March.....	46
Figure 4.2: Precipitation Anomaly for the Months of April, May, and June	47
Figure 4.3: Precipitation Anomaly for the Months of July, August, and September	48
Figure 4.4: Precipitation Anomaly for the Months of October, November, and December ...	49
Figure 4.5: Calibration Optimization Simulation Element	51
Figure 4.6: Calibration of HEC-HMS using Observed River Discharge Data at 1KB05	52
Figure 4.7: Validation Optimization Simulation Element.....	52
Figure 4.8: Validation of HEC-HMS using Observed River Discharge Data at 1KB05	53
Figure 4.9: Pearson Correlation Coefficient between Precipitation and River discharge.....	54
Figure 4.10: Standardized Hydrometric Indices for the January, February, and March.....	55
Figure 4.11: Standardized Hydrometric Indices for the April, May, and June	55
Figure 4.12: Standardized Hydrometric Indices for the July, August, and September.....	56
Figure 4.13: Standardized Hydrometric Indices for the October, November, and December	56
Figure 4.14: Return Period of the Independent Flood Magnitude at G-M River Basin.....	57
Figure 4.15: The percentage of percentage Annual Exceedance Probability	58
Figure 4.16: Flood Frequency Estimates by the Selected Probability Distribution Curves....	60
Figure 4.17: Performance comparison of the four Probability Distribution Models.....	61
Figure 4.18: Probability Distribution Model for Gucha-Migori River Basin	64
Figure 4.19: Performance Efficiency of Various NAR Models	65
Figure 4.20: L-M algorithm MSE Output	67
Figure 4.21: Error Histogram for the NAR Model	67
Figure 4.22: Regression of the best Nonlinear Autoregressive Neural Network	68

Figure 4.23: Time-Series Response of Nonlinear Autoregressive Neural Network..... 69
Figure 4.24: Error Autocorrelation of trained Nonlinear Autoregressive Neural Network 70
Figure 4.25: Forecasted Flood Magnitudes and their Frequencies 70

LIST OF SYMBOLS

Symbol	Description
b	Bias at the cell body
$f(x)$	Gamma function
$g(x)$	Gamma distribution
m	Number of hidden neurons
n	Number of input neurons
W_i	Weight attached to the input signal i
X_i	An input vector
R^2	Coefficient of Determination
α	Significance level
p	Probability values
r_{-}	Substitution of a parameter by a value
v_{-}	Relative change in a parameter
$f(.)$	Activation function
NSE	Nash Sutcliffe model efficiency
Sim	Simulation
CV(t-p)	Feedback delay
Z_c	Calculated standard normal distribution test statistics

LIST OF ABBREVIATIONS AND ACRONYMS

AEP	Annual Exceedance Probability
ANN	Artificial Neural Network
AMJ	April, May, June
CS	Climatic Scenario
DEM	Digital Elevation Model
FAO	Food and Agriculture Organization of the United Nations
FNN	Feedforward Neural Network
GUM	Gumbel
HEC-HMS	Hydrologic Engineering Centre - Hydrologic Modeling System
HEC-GeoHMS	Hydrologic Engineering Centre -Geospatial Hydrologic Modeling
HRU	Hydrologic Response Unit
IPCC	Intergovernmental Panel on Climate Change
JFM	January, February, March
JAS	July, August, September
LP3	Log Pearson type III
LULC	Land Use-Land Cover
MSS	Multi-Spectral Scanner
OND	October, November, December
PD	Probability Distribution
SCS-CN	Soil Conservation Service Curve Number
SRTM	Shuttle Radar Topography Mission
SUFI-2	Sequential Uncertainty Fitting 2
SDG	Sustainable Development Goals of the United Nations
SWAT	Soil and Water Assessment Tool
TM	Thematic Mapper
USGS	United States Geological Survey
UTM	Universal Transverse Mercator
UNEP	United Nations Environmental Programme
UNFCCC	United Nations Framework Convention on Climate Change
WGEN	Weather Generator
WMO	World Meteorological Organisation

CHAPTER ONE

INTRODUCTION

1.1 Background Information

Climate change and growing socio-economic developments continue to alter hydrological regimes and the response of several watersheds globally, thus threatening water energy, and food security (Archer et al., 2010; IPCC, 2014; UNFCCC, 2005; Wambua et al., 2017). In Kenya, there is a study recognition of ecosystem deterioration, spatial and temporal uncertainties in water input of various basins, and changes in watershed storage, which further aggravate extreme hydrological events like floods (Juma et al., 2020; Opere, 2013). The aforementioned challenges accelerate flood scenarios because such extreme hydrologic events depend entirely on parameters that include soil antecedent moisture, land use system, catchment area, and rainfall patterns (Gichere et al., 2013). Furthermore, flooding is usually caused by highly intense and continuous rainfall occurring for an extended duration, which then exceeds the infiltration capacity of soil or flow capacity of coastal regions, rivers, and streams resulting in runoff (Thavhana, 2018).

Surface runoff can be through Hortonian or saturation overland flow. Hortonian overland flow is generated when the intensity of rainfall exceeds the infiltration capacity of the soil, while saturation overland flow is produced when subsurface flow saturates the soil near the bottom of hill slopes and near stream banks. The runoff produced may then cause the catchment to respond in a manner that results in flooding (Singo et al., 2012; Warburton et al., 2010). Adero (2017) explains that flood occurrence in the Gucha-Migori River Basin is a result of heavy rains upstream that lead to heavy surface run-off flow into both the Gucha and Migori river systems. The surface run-off erodes soil as it flows into the river leading to heavy sedimentation of the river channel as the water flows downstream.

On the other hand, the flood-plain area also experiences flash floods from the neighbouring hills within the Lower Gucha Migori Sub-catchment and this leads to the loss of crops and disruption of agricultural activities (Muiruri et al., 2014; Ogembo, 2018). The flood hazard events prevalence rate in Kenya stands at 27% and affects more than 5% of the population (Akello, 2014). Besides, the United Nations Environmental Programme (UNEP, 2010) points out that flood-related fatalities constitute over 60 % of disaster victims in Kenya. Several studies report that flood hazards have increased in number, frequency, and complexity in many parts of Kenya including the Gucha-Migori River Basin (Adero, 2017; Gaya, 2020; Ogembo,

2018; Opere, 2013; Quandt & Kimathi, 2017). The level of destruction has also become more severe and poses consequences on agricultural activities, water resources management, human health, development of engineering projects, wildlife, hydropower generation, and forestry (Akello, 2014; Gaya, 2020). It then implies that strategies addressing flood-related challenges are critical for the realisation of Kenyan's big four agenda, Sustainable Development Goal (SDG) number 1, 2, 3, 13, and 16, and Vision 2030.

The common strategies and mitigation measures for coping with floods involve warnings as well as the construction of flood protection structures especially dykes and dams (Gaya, 2020). It encompasses relevant attempts for mitigation against the impacts of flood damage, which include disruption of the daily livelihoods, and enlighten schemes that make it easier and faster life-skills in recovery from the flood damage. However, WMO (2011a, b) illustrates that in the course of drawing up the flood management plans, the appropriate combination of structural and non-structural measures should be considered. Non-structural flood mitigation measures encompass all activities focused on land-use regulations, hydrologic modelling, disaster prevention, flood-proofing, continuous forecasting, and flood frequency analysis. Moreover, their implementation requires the application of modern techniques, which should describe, analyse spatially and temporally, simulate, and integrate forecasted flood magnitudes with other related information.

Non-structural methods make it possible to monitor the progress of floods in near real-time and to produce accurate, rapid, and cost-effective mapping of floods (Gaya, 2020). The coupling of hydrologic models and flood frequency distribution techniques would therefore provide a hybrid tool for the simulation of flood events. Thus, this study focuses on modelling flood discharge using a hydrologic model (HEC-HMS), and the integration of the PD model with an artificial neural network for frequency analysis and forecasting of the events in the Gucha-Migori River Basin. The study seeks to provide useful insights, knowledge, and data products, which may enhance the probability of establishing that a flood of a given magnitude will hit during any particular year. Further, such a study is necessary for basin rehabilitation, and monitoring as well as the design of suitable approaches for integrated water resource management (Birkholz et al., 2014; Hansson et al., 2008).

1.2 Statement of the Problem

Floods are the most devastating natural disaster frequently occurring in catchments within the Gucha-Migori River Basin nearly every year according to the JICA draft report on integrated

flood management plan (2014) and the local water resource authority. Previous studies such as Adero (2017), Gaya (2020), and Ogembo (2018) reveal that trends in flood magnitude, frequency of occurrence, and damages have progressively increased during the last decades. Although flood risk resilience has been conducted by the Water Resources Authority using structural developments and consensus-building approaches, these methods alone have proven insufficient in effectively mitigating the adverse impacts of floods.

The increasing frequency and severity of floods necessitate a shift towards non-structural interventions, which are essential for comprehensive flood management. Non-structural methods include land-use regulations, hydrologic modelling, disaster prevention, flood-proofing, continuous forecasting, and flood frequency analysis. These approaches provide more flexible, adaptive, and sustainable solutions by emphasizing preparedness, early warning systems, and real-time flood monitoring. Integrating non-structural methods with structural measures enhances the overall resilience of the flood management strategy and supports the sustainable development goals.

This study explores the need for non-structural interventions by focusing on hydrologic modelling, quantification of the response to flood events, and prediction of flood occurrence probabilities using probability distribution functions and artificial neural networks. The implementation of these advanced techniques aims to address the knowledge gap regarding future flood scenarios in the basin, thereby improving flood management strategies and enhancing community resilience within the Gucha-Migori River Basin. This integrated approach is critical for basin rehabilitation, monitoring, and the design of effective water resource management plans.

1.3 Objectives

1.3.1 Broad Objective

The broad objective was to model and forecast flood events in the Gucha-Migori River Basin for decision support in integrated water resource management.

1.3.2 Specific Objectives

The specific objectives were to:

- i) Determine the response of river discharge to precipitation variability for the period 1969 to 2015 using the HEC-HMS model
- ii) Determine the relationship between flood discharge magnitude and frequency using the appropriate probability distribution model

- iii) Forecast flood magnitudes and P-percent annual exceedance probabilities for the period (2015 – 2052) using an artificial neural network and probability distribution model

1.4 Research Questions

- i) How does precipitation variability influence river discharge over the period 1969 to 2015, as simulated by the HEC-HMS model?
- ii) How do flood magnitude and frequency relate based on probability distribution models?
- iii) How will flood magnitudes and probabilities of exceedance vary for the period between 2015 and 2052?

1.5 Justification

The impact of flood events adversely affects livelihoods, its' complex and highly uncertain and has the potential to influence relatively stable socio-economic activities to a precarious situation and jeopardize basin management plans. Therefore, modelling the response of flood events to precipitation variability is important for basin rehabilitation and the design of strategic approaches for integrated flood implementation plans. Analysis of flood frequency and probability distribution curves provide data products for the design of hydraulic structures, floodplain zoning, and the creation of system operational plans. Flood forecasting creates a reasonable design criterion for water resources projects, thus, reducing projects' cost, and rationally saving lives, properties, and socio-economic activities.

The selection of the Hydrologic Engineering Center's Hydrologic Modeling System (HEC-HMS) for this study is based on its proven capabilities and widespread application in hydrologic modeling, particularly in simulating river discharge responses to precipitation events. HEC-HMS has been extensively used in various hydrologic studies globally and has demonstrated high efficacy in simulating hydrologic processes in river basins. Its application is well-documented in numerous studies, including those conducted in Kenya's Nyando, Ruiru, Kuja, Mkurumudzi, and Uмба river basins (Ismael et al., 2017; Ogembo 2018; Olang & Fürst 2011; Ouédraogo et al., 2018; Tesfamariam et al., 2021),

Furthermore, HEC-HMS is preferred over other models due to its balance between being physically-based and less demanding on input data compared to fully distributed models (Bhuiyan et al., 2017; Gyawali & Watkins, 2013; Thu et al., 2019). This makes it a practical choice for regions where comprehensive data collection is challenging. HEC-HMS's ability to model various hydrologic processes, including precipitation, infiltration, surface runoff, and

channel routing, ensures that all significant aspects of the hydrologic cycle are captured. This makes it highly effective for flood forecasting and water resources management.

Additionally, probability distribution curves are employed in this study to statistically analyse and predict extreme hydrologic events. These curves are vital for understanding the frequency and magnitude of flood events, thereby providing essential insights for flood risk management. Probability distribution curves help in quantifying the likelihood of various discharge levels occurring, which is crucial for designing infrastructure and implementing mitigation measures. The use of probability distributions, such as the Log-Pearson Type III distribution, is standard practice in hydrology for modeling flood frequency and assessing return periods of extreme events (Engeland et al., 2004; Hussain et al., 2018; Kumar, 2019).

Moreover, artificial neural networks are integrated into this study to enhance the prediction accuracy of hydrologic responses to precipitation variability. ANNs are particularly effective in capturing non-linear relationships between input variables and hydrologic responses, which traditional models may not adequately represent. The flexibility and adaptability of ANNs make them powerful tools for forecasting river discharge, especially when dealing with complex and highly variable hydrologic data (Dawson & Wilby, 2001; Maier & Dandy, 2000). By training the neural network with historical precipitation and discharge data, the model can learn patterns and improve its predictive performance, thus offering a complementary approach to traditional hydrologic models.

In conclusion, the choice of HEC-HMS, probability distribution curves, and artificial neural networks for this study is justified by their extensive application in similar studies, their capability to handle complex hydrologic processes with relatively moderate data requirements, and their robust frameworks for simulation, calibration, validation, and prediction. These methods and models collectively provide a comprehensive toolkit for investigating river discharge responses to precipitation variability and contribute valuable insights into flood water resources planning and management.

Therefore, employing advanced modeling techniques such as the HEC-HMS model, artificial neural networks, and probability distribution models, this research contributes to global efforts in flood risk management and disaster preparedness. Accurate flood predictions will benefit local communities in Kenya while also providing insights applicable to other flood-prone regions worldwide. The findings support global initiatives in IWRM, helping to achieve

Sustainable Development Goal (SDG) 13 on climate action and SDG 6 on ensuring the availability and sustainable management of water resources.

1.6 Scope and Limitations of the Study

The study area covers only the Gucha-Migori River Basin. HEC-HMS model was used for flood simulation for the period (1969-2015). For the spatial data (Digital Elevation Model, Land Cover, and Soil Maps), it was assumed that the processed datasets have the same characteristics as the real physical features. Further, the study focused on the integration of the Probability Distribution model with the Artificial Neural Network Model to forecast flood magnitudes and their respective P-percent annual exceedance probabilities.

1.7 Definition of terms

Artificial Neural Network	A data-centric procedure employing a flexible mathematical algorithm or a mimicry of the biological nervous system that possesses the ability to address intricate nonlinear associations.
Climate	The statistical representation in terms of the variability and the mean of relevant variables or average weather over a duration ranging from weeks to millions of years, i.e. it is the weather conditions prevailing in an area over a long period of time.
Climate variability impact	The enduring impacts or outcomes of climate fluctuations that extend beyond singular weather occurrences.
Precipitation variability	Describes how precipitation may fluctuate over time and tells us how big the difference between wet and dry conditions in a particular place could be.
Flood Event	The inundation of a dry place caused by overflowing water in an existing waterway such as a stream, river, or drainage ditch.
Forecasting	Forecasting future states of a phenomenon, system, or quantity by leveraging information about its current and past states, frequently achieved through the use of a model.
HEC-HMS Model	A model developed by the US Army Corps of Engineers of the Hydrologic Engineering Center (HEC), which contains an integrated tool for simulating hydrologic variables of the dendritic river basin.

Hydrologic Modelling	The description of actual hydrological attributes and systems through the utilization of computer simulations, mathematical counterparts, and miniature physical replicas.
Land cover	The ground's outer layer, encompassing elements such as vegetation, urban structures, bodies of water, exposed soil, and more.
Land use	The function that the land fulfils, such as providing opportunities for recreation, serving as a habitat for wildlife, or supporting agricultural activities.
River Discharge	The volume of water flowing through a river channel; measured at any given point in cubic meters per second

CHAPTER TWO

LITERATURE REVIEW

2.1 Flood

According to Bourenane et al. (2019), a flood is an overflow of water that submerges land, which is usually dry, or an abnormal progressive rise in the water levels of rivers or channels that may result in an overflow. The overflow is mainly due to runoff response to changes in upstream land use, heavy precipitation, a storm surge from a tropical cyclone, and continuously increasing population and assets in flood-prone areas (Sriwongsitanon & Taesombat, 2011; Viglione et al., 2009). In hydrology, such response of runoff to human induced land use change and precipitation characteristics can further be illustrated by flood hydrograph as shown in Figure 2.1

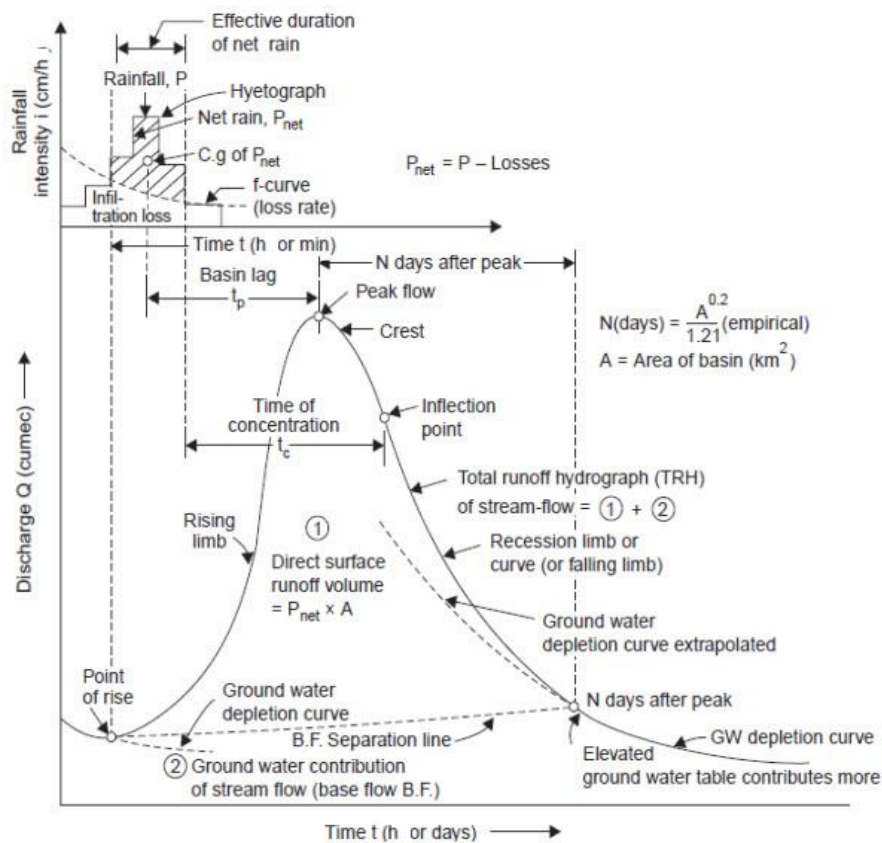


Figure 2.1: Flood Hydrograph

Source: Raghunath, (2006)

In a broader perspective, the flood hydrograph (Figure 2.1) shows how a drainage basin responds to a period of rainfall. Rising limb, excess rainfall, peak discharge, and falling limb respectively indicate an increase in river discharge, excess runoff, time when the river reaches

its highest flow, and runoff is still reaching the river but in decreasing amounts (Albishi et al., 2017; Raghunath, 2006). It implies that a gentle hydrograph shows the river is at low risk of flooding, which means that it takes longer for the peak rainfall to reach the river channel, so the river discharge is increasingly slow. Floods can be categorised into river floods, coastal floods, storm surges, inland flooding, and flash flood (Jonkman & Vrijling, 2008; Perry, 2000). However, USGS illustrates that there exist two basic types of floods, namely, widespread river floods and flash floods. Some researchers like Booij (2005) and Douben (2006) describe river flooding to be a common natural disaster for large rivers in areas with heavy precipitation, in the event where excessive runoff from longer-lasting rainstorms causes a water-level rise for a relatively longer duration over a larger catchment.

Other studies (Dottori et al., 2018; Jongman et al., 2012) point out that river floods can occur slowly or abruptly, where, sudden runoff events happen more frequently on normally dry channels, rivers that flow for much of their length over impermeable terrain, and rivers with steep valleys. On the other hand, flash floods occur when runoff from excessive precipitation causes a rapid rise in the water height of a normally dry channel or stream in a short amount of time sometimes limiting the time available to warn and protect the public (Davis, 2001).

The assertion by Collier (2007) and Hapuarachchi et al. (2011) further demonstrate that flash flood is accompanied by other phenomena like psychological harm to people, damage to properties and businesses, bridge collapse, landslides and mudflows, and, in exceptional circumstances, fatalities. Exacerbated anthropogenic activities and climate change indicate an increase in watershed degradation and the intensity of rainfall posing a potential influence on runoff generation in many parts of the world including Kenya, which may lead to more severe flash flooding (Mishra et al., 2018; Ogembo, 2018; Rwigi, 2014).

2.2 Response of Flood Events to Precipitation Variability

Changes in climate and land-use systems alter the hydrologic regime of a basin by changing precipitation partitioning, which brings about extreme variations of subsurface flows, groundwater flows, and surface runoff (Amisi et al., 2020; Schipper, 2017). Such changes bring different responses of runoff, which may then contribute to flooding events because precipitation variability and changes in the Land-use system occur at different spatial and temporal scales. Besides, the impact of changes in precipitation and LULC might compensate for or strengthen each other. On the other hand, some researchers like Renner et al. (2014) explain that they both might occur in parallel.

For instance, Mwetu (2019) analysed the influence of land cover changes and climate variability on the discharge regime of Njoro River Catchment, Kenya. Results showed a negative trend of annual discharge that corresponded to increased deforestation, open fields, bare land, and grassland. Further analysis pointed out that human activity mainly deforestation accounted for 75% of the reduction of discharge while precipitation variability accounted for 25% of the reduction of discharge. This implies that land-use changes were largely responsible for runoff, which in turn would then potentially contribute to flooding events.

Although there have been several studies conducted on the surface runoff response to changes in LULC, the evidence from some studies is still contradictory. For example, other researchers elaborate that an increase in the annual discharge is caused by a reduction of forest cover (Dias et al., 2015; Farley et al., 2005; Hayhoe et al., 2011). On the other hand, studies like Githui et al., (2009), Kundu (2007), Mwetu (2019), and Rodriguez et al. (2010) postulate that land-use changes from forest to mixed rural built-up lands and subsistence agriculture causes the increase of runoff but deteriorates subsurface as well as groundwater flows.

However, the aforementioned responses of surface water circular are based on the fact that LULC influences soil physical properties, available water content, infiltration capacity, and saturated hydraulic conductivity. This would mean that the changes in the land-use system might significantly influence flood magnitude, time, and spatial variation.

For example, Olang and Fürst's (2011), analyses on the effect of LULC on flood peak discharges and runoff volumes in Nyando River Basin, Kenya using HEC-HMS successfully outlined the hydrologic consequences of the eminent land cover changes. The model results further demonstrated that with higher rates of upstream deforestation, the runoff and flood peak discharges and volumes increased by at least 10 % in the entire basin. Such findings are consistent with many studies like Brody et al. (2014), Hussein et al. (2020), and Szwagrzyk et al. (2018). Conversely, Kabeja et al. (2020) evaluated the impact of reforestation-induced LULC on flood peak discharge using HEC-HMS. Their results pointed out that the reforestation resulted in a decrease in flood peak discharge ranging from 14-16%.

Although changes in LULC influence runoff and flood magnitudes, the main dominant factor in the basin affecting the spatial and temporal distribution of flood routing processes is precipitation variability (Davenport et al., 2021). For instance, Tabari (2020) quantified the response of flood intensities to changes in extreme precipitation and found that extreme storm events intensified flood volumes with the seasonal cycle of water availability. Similarly,

Chegwidden et al. (2020), Fang et al. (2021), and Gandini et al. (2020) have also reported a stronger relationship between precipitation and flood events. Also, for the runoff analysis, Ogembo (2018) carried out hydrologic modelling and climate change studies on River Kuja Basin using HEC-HEC-GeoHMS and reported that both Runoff and precipitation showed a downward trend analysis.

The analysis by Ogembo (2018) revealed a significant decline in runoff in drier months compared to wetter months and concluded that there will be a high risk of flash floods in the future but consequently very low discharges during dry seasons. A similar response has also been reported by Amisi et al. (2020), Mango et al. (2010), Mwangi et al. (2016), and Rwigi (2014). It implies that direct runoff is a result of the spikes caused by a rainstorm, which then contributes to peak flow, hence river or flash floods.

Therefore, it can be inferred that precipitation variability influences the variation in spatial redistribution, time, frequency, and magnitude of floods. Therefore, it is imperative to note that the response of flood routing events to precipitation variability is complex, uncertain, and varies spatio-temporally, and hence may only be simulated in most cases by hydrologic models (Devia et al., 2015; Mwangi et al., 2016; Mwetu, 2010).

2.2.1 Hydrologic Modelling

Hydrologic modelling is the characterization of real hydrologic features and systems by the use of computer simulations, mathematical analogues, and small-scale physical models (Devia et al., 2015). Hydrologic models can broadly be classified into stochastic and deterministic models. Stochastic models possess inherent randomness, where the same set of parameter values and initial conditions will lead to an ensemble of different outputs, while in deterministic models, the output is fully determined by the parameter values and the initial conditions (Farmer & Vogel, 2016).

Marhaento et al. (2016) elucidate that hydrologic models are vital to the optimization and operation of water resources, and this explains why many statistical, empirical, and conceptual discharge prediction models have been developed for decision support in water management. However, statistical techniques, such as linear regression-based approaches are constrained, simplistic, and have limited capacity to handle non-linear relationships (Amisi et al., 2020).

Conceptual hydrologic models are usually considered the best alternative because they take into account hydrologic processes through mathematical formulations (Devia et al., 2015). The

law of conservation of mass and momentum energy guides the development of conceptual hydrologic models since most physical modelling includes storage of water, the spatial and temporal distribution of flows, and occurrence. These laws can be expressed by the concept of continuity and momentum Equations (2.1 and 2.2). The equations are applied in modelling under the assumption that the flow is unidirectional, the fluid is incompressible, vertical accelerations are negligible and hydrostatic pressure prevails.

$$\frac{\partial A}{\partial t} + \frac{\partial (vA)}{\partial x} - q = 0 \quad (2.1)$$

$$\frac{\partial Q}{\partial t} + \frac{\partial (vQ)}{\partial x} + gA \left(\frac{\partial y}{\partial x} - s_0 + s_f \right) = 0 \quad (2.2)$$

where, q is the lateral inflow (m^3), Q is the discharge in the channel (m^3/s), A is the area of flow in the channel (m^2), n is Manning's coefficient for the channel, S_0 is the bed slope (m/m), and S_f is the friction slope of the channel (m/m).

Many researchers and organisations affirm the importance of conceptual hydrologic models such as SWAT, HRDROTEL, HEC-HMS, WATFLOOD, MIKE11/SHE, SPHY, WEAP, and TOPMODEL in the vital role they play in integrated water resources management solutions. Out of all the conceptual models, HEC-HMS has been demonstrated to be the most preferred model for flood routing processes simulation (Fleming, 2004; Natarajan & Radhakrishnan, 2019; Oleyiblo & Li, 2010; Thakur et al., 2017). HEC-HMS has been widely used because it is more physically based than the structure of lumped models, and they are less demanding on input data than fully distributed models (Bhuiyan et al., 2017; Gyawali & Watkins, 2013; Thu et al., 2019). Besides, it explains why the HEC-HMS model has been applied successfully in many River basins in Kenya which include Nyando (Olang & Fürst, 2011), Ruiru (Ismael et al., 2017), Kuja (Ogembo, 2018), Mkurumudzi (Ouédraogo et al., 2018), and Uмба (Tesfamariam et al., 2021).

2.2.2 Hydrologic Engineering Centre - Hydrologic Modeling System (HEC-HMS)

Hydrologic Engineering Center (HEC-HMS) is a model developed by the US Army Corps of Engineers of the Hydrologic Engineering Center (HEC), which contains an integrated tool for simulating hydrologic variables of dendritic river basin systems. It is a physically-based semi-distributed, event-scale hydrologic model used to represent hydrological processes (Chu & Steinman, 2009; Du et al., 2019). As further illustrated by Fleming (2004), the construction of

the HEC-HMS model for simulation involves dividing an entire river basin into homogeneous sub-basins based on the defined drainage area threshold. The mass flux and energy balances within the hydrologic cycle are then modelled using mathematical equations.

HEC-HMS model requires spatial data (digital elevation model, LULC, and Soil maps), meteorological, and hydrologic datasets (Ouédraogo et al., 2018). The spatial data is prepared and processed from HEC-GeoHMS and imported to the HEC-HMS model to simulate flow, stage, and timing for the river basin. Therefore, the HEC-HMS model has three major components namely, control specification, meteorological model, and basin model (Ramly & Tahir, 2016). The meteorological model consists of the precipitation and evaporation datasets, the control specification contains calculation intervals for the run, while the basin model contains elements of the sub-basin, the connectivity, and the runoff parameter. HEC-HMS model consists of the following components for the simulation of the runoff response to precipitation (Gebre, 2015; Ogembo, 2018). Precipitation specification option, which describes the historical data at a given location.

The second component is the loss models that approximate the runoff magnitudes given precipitation datasets and river basin characteristics. Other components include direct runoff models that account for overland flow, energy losses, and storage, and the hydrologic routing models, which account for energy flux and storage during the period water flows through the stream channels. Some of the additional models are those for naturally occurring confluences and bifurcations, and models of water control measures. The HEC-HMS model contains eight elements, which include the diversions, reservoir, sink, source, junction, reach, and sub-basins (Ogembo, 2018; Ramly & Tahir, 2016).

Every sub-basin has corresponding precipitation thus the outflow for the element is computed through the subtraction of the precipitation losses. Surface runoff is then calculated and the base flow is added. The reach element conveys the river discharge to the basin model and the inflow into the reach is obtained from the upstream elements. Translation and attenuation should be accounted for then outflow from the reach is calculated. Figure 2.2 shows an overview of the rainfall-runoff process simulation in HEC-HMS.

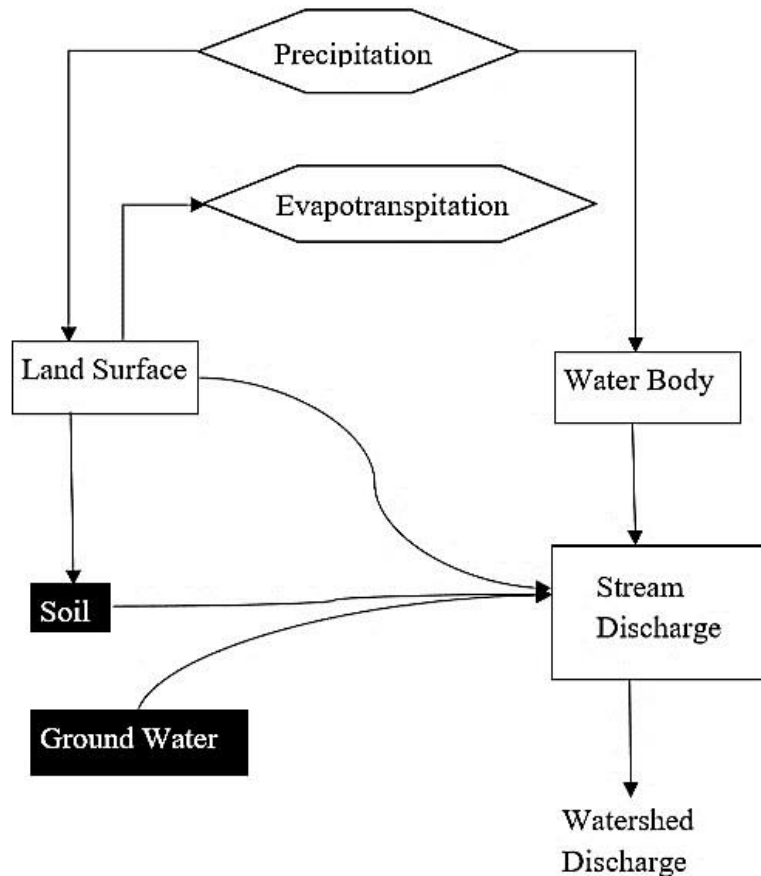


Figure 2.2: Schematic Diagram of the Rainfall-Runoff Process in HEC-HMS

Source: Ogembo, (2018)

All the inflow into the junction must be summed up to obtain the outflow, and the source element introduces inflow into the basin model. However, the outflow of the source element may be defined by the user, and hence the sink element is used to represent the outlet of the basin. The reservoir element models the hydrograph detention and attenuation as a result of the detention pond. Computation of the outflow from the reservoir can be achieved by applying any of the routing approaches in HEC-HMS (Fleming, 2004; Ogembo, 2018).

The diversion element models the discharge leaving the main channel, and its inflow can be obtained from many upstream channels, it should be noted that computation of the diverted flow can be done using the user's input. Finally, the non-diverted and diverted can be connected to other hydrologic elements located downstream of the diversion elements (Scharffenberg & Fleming, 2005).

2.2.3 Hydrologic Engineering Centre -Geospatial Hydrologic Modeling Extension

HEC-GeoHMS is an extension for ArcGIS released by the US Army Corps of Engineers, Hydrologic Engineering Center (HEC) (Fleming, 2004; Tesfamariam et al., 2021). It is a toolkit of geospatial hydrology, which allows operators to process and create basin parameters based on the topographic data for hydrologic modelling (USACE, 2010). In addition, HEC-GeoHMS processes geospatial data and creates their input files in ArcGIS for HEC-HMS. Figure 2.3 adapted from USACE (2013) shows the relationship between GIS, HEC-GeoHMS, and HEC-HMS.

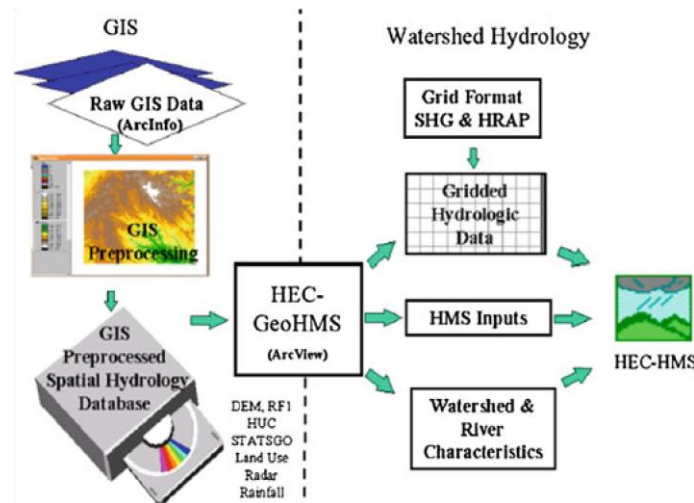


Figure 2.3: Overview of HEC-GeoHMS Program

Source: USACE, (2010)

HEC-GeoHMS is applied to derive a river network of the basin from the digital elevation data. To obtain a digital elevation model to demarcate various components of the catchment, some of the major steps undertaken include filling sinks, flow direction derivation, demarcation of basin and sub-basin, calculation of flow accumulation, and stream network definition (USACE, 2013). HEC-GeoHMS creates the drainage network by analysing the digital terrain data and transforming the drainage paths and basin boundaries into a hydrologic data structure.

2.2.4 HEC-HMS Model Calibration and Validation

The successful application of hydrologic models including HEC-HMS depends on how well calibration and validation are achieved. Calibration is the process of minimizing the model output uncertainties before running simulations by adjusting parameters to best capture the local conditions (Abbaspour et al., 2007; Arnold et al., 2011; Kamali et al., 2013). However, validation is the running of the model with calibrated parameters in an independent data mass

so that the applicability of the model can be assessed through statistical tests. For the HEC-HMS model, manual calibration is performed by visual inspection and trial and error-based procedures. (Kamali et al., 2013). Some studies such as Dariane et al. (2016) and Odyuo (2020) point out that manual calibration can be tedious, time-consuming, and may require experience and experimental information. Auto-calibration is based on systematic techniques to find the best parameter values based on pre-defined objective functions, thus, more likely to produce better results (Dariane et al., 2016; Kamali et al., 2013; Sardoii et al., 2012).

Some of the widely applied auto-calibration techniques for the HEC-HMS model entail Sequential Uncertainty Fitting 2 (SUFI-2), Genetic Algorithm (GA), Nelder-Mead (NM), and Univariate-Gradient (UG), Melody Search Algorithm (MeS), Self-Adaptive Global Harmony Search (SGHS). Several studies have highlighted various aspects and challenges inherent in the aforementioned auto-calibration approaches such as parameterization, non-uniqueness of parameter values (Abbaspour et al., 2004), and data quantity and quality (Perrin et al., 2007). Also, the type and the number of objective functions and their characteristics (indifference to parameter values, non-convexity, and multi-modality) (Kamali et al., 2013), and the performance of the optimization algorithms (Ndiritu, 2009). The methodology for addressing uncertainty, sensitivity, calibration, and validation has been detailed. Specific techniques used, parameters tested, and evaluation criteria are explained to ensure robustness and reliability of the model.

For instance, studies by Kamali et al. (2013) preferred the use of a multi-objective to Particle Swarm Optimization (PSO) algorithm for automatic calibration of HEC-HMS. According to Dariane et al. (2016), the Genetic Algorithm is preferred to Nelder-Mead and Univariate-Gradient when using a snowmelt module in a continuous model for enhancement of efficiency. Many researchers such as Abbaspour et al. (2015), Kumar et al. (2020), and Mousavi et al. (2012) recommend the SUFI-2 algorithm due to its higher performance in terms of adjusting model parameters to mimic real hydrologic conditions.

2.2.5 Hydrologic Model Performance Assessment

A wide range of statistics has been used to evaluate HEC-HMS hydrologic predictions. By far the most widely used statistics reported for hydrologic calibration and validation are Coefficient of Determination (R^2), and the Nash Sutcliffe model efficiency (Nash). The R^2 measures how the observed versus simulated regression line approaches an ideal match (Fernandez et al., 2005). R^2 values range from zero to one, with a value closest to zero

indicating no correlation while a value closest to one indicating relative perfect linear covariation between the two datasets. It implies that a correlation measurement reveals the high accuracy of the model when the value is approaching one.

Nash Sutcliffe model efficiency ranges from $-\infty$ to 1 and measures how well the observed and simulated data match the 1:1 line (Moriassi et al., 2007). The values of Nash closer to zero or equal to 0 indicate that the mean of the observed data is a better predictor than the model, and the values closer to one or 1 imply a perfect fit between the observed and simulated. Considering various time steps of modelling, the performance evaluation of the hydrologic model under the defined values of Nash and R^2 can be rated as per the recommendations by Fernandez et al. (2005) and Moriassi et al. (2007) (Table 2.1). Practical recommendations for future research and water resource management have been provided. These include specific areas for further investigation and actionable advice for policymakers to improve flood management and mitigation strategies.

Table 2.1: General performance ratings for recommended statistics

Nash	R^2	Rating
75.0% Nash \leq 100%	75.0 % $< R^2 \leq$ 100 %	Very good
60.0 % $<$ Nash \leq 75.0%	60.0% $< R^2 \leq$ 75.0 %	Good
36.0 % $<$ Nash \leq 60.0 %	50.0% $< R^2 \leq$ 60.0 %	Satisfactory
0.0 % $<$ Nash \leq 36.0 %	25.0 % $< R^2 \leq$ 50.0 %	Poor
Nash \leq 0.0%	$R^2 \leq$ 25.0 %	Inappropriate

Note. Modified from Van Liew et al. (2003) and Singh et al. (2004).

This study discusses the use of the HEC-HMS model for flood simulation (Ikhwali et al., 2022; Ismael et al., 2017). While HEC-HMS is a widely used tool, the review does not sufficiently critique its limitations, such as its performance in different geographic settings or its dependency on high-quality input data, which may not always be available. For example, the HEC-HMS model, though superior in its physical basis compared to other lumped models, relies heavily on detailed and accurate input data, including digital elevation models (DEM), land use/land cover (LULC), and soil maps. In regions where such data is scarce or outdated, the model's accuracy can be significantly compromised.

However, the application of the HEC-HMS model in different hydrological and climatic contexts has revealed varying degrees of effectiveness. Studies have shown that the model's calibration and validation processes are essential to ensure reliable simulation results (Darlane

et al., 2016; Odyuo, 2020). However, manual calibration, often employed in these studies, is not only labor-intensive but also subjective, leading to potential inconsistencies in the results. Auto-calibration methods, while more systematic, may still fall short in capturing the unique hydrological characteristics of diverse river basins.

Despite these challenges, HEC-HMS remains a popular choice for flood modeling due to its balance between physical representation and data requirements. Its integration with GIS through the HEC-GeoHMS extension further enhances its utility by allowing for detailed spatial analysis and visualization. However, further studies need to be done to address the need for continuous updates and improvements in input data and the calibration process to maintain the model's accuracy and applicability across different settings.

2.3 Flood Frequency and Probability Distribution Models

Flood frequency analysis and probability distribution models involve the concept of modelling the relationship between magnitude and recurrence interval from the available data, using various techniques to estimate at least roughly, how big the projected flood is, in a decade, century, or a millennium (Lang et al., 2010; Rizwan et al., 2018). According to Şen (2018) and Zischg et al. (2018), a flood can be characterized by magnitude, how severe or large a flood event is. Discharge is the common measure of flood magnitude or how much water in the streambed is flowing past a certain point in a given duration (Ghosh, 2013; Zischg & Bermúdez, 2020). To estimate the flood magnitude, total runoff volumes are measured for the flood hydrograph above the baseline discharge using a threshold discharge of a specific recurrence interval flow.

The calculated magnitude value becomes the runoff volume accumulated, compared to the flood volume of the record. To obtain total runoff volumes, daily runoff values are summed once discharge exceeds the threshold, and the sum is multiplied by contributing watershed area to measure total flood runoff volume. Therefore, it implies that annual peak-flow data collected or simulated provides an estimate of the flood magnitude as well as the frequency at a particular basin outlet. A longer-duration flood exhibits a higher flood magnitude, which would mean that flood volumes would be larger from the larger watersheds if other factors are constant (Gotvald et al., 2012). Nonetheless, Ghosh (2013) and Şen (2018) hold the view that river and watershed size does not affect the magnitude number.

2.3.1 Flood Frequency

The terminology associated with flood frequency estimations is shifting away from the T-year recurrence interval flood to the P-percent annual exceedance probability (AEP) flood (Gotvald et al., 2012). AEP is currently preferred because it conveys the probability, or odds, of a flood of a given magnitude being equalled or exceeded in any given year. For instance, a 1-percent AEP flood usually known as the 100-year flood corresponds to the flow magnitude that has a 0.01 probability of being equalled or exceeded in any particular year. The P-percent annual exceedance probability is calculated as the reciprocal of the recurrence interval (T) multiplied by 100.

Recurrence intervals (flood frequencies) or return period which means the average number of years between one flood of a given magnitude and the next flood that is as big or bigger can be described statically as follows.

Taking (X) as a random variable that has a cumulative distribution function $F_x(x)$. The probability that (X) is less than equal to a given event (x_p) is given as:

$$F_x(x) = P(X \leq x_p) = p \quad (2.3)$$

The probability that this event will be exceeded is then equal to $1-p$ and the percent exceedance is denoted as $100(1-p)$. For such an event x_p , the return period corresponding to this exceedance probability is denoted by T .

$$\text{Here, } T = \frac{1}{(1-p)} \quad (2.4)$$

From this statistical description, the 100-year return period of the flood may then be understood as an event with a probability of exceedance $1-p = (0.01)$ or a non-exceedance probability ($p = 0.99$). Moreover, it would also imply that there is a 99 % chance that this event will not be exceeded within a particular year.

2.3.2 Probability Distribution Functions (PDFs)

Table 2.2 shows the probability distribution models and their parameters, which are usually applied in flood forecasting.

Table 2.2: The parameters and PD functions

Number	Distribution	Probability Density Function	Parameters
1	GAM	$F(x) = \frac{x^{\alpha-1} \exp\left(\frac{-x}{\beta}\right)}{\beta^{\alpha} \Gamma(\alpha)}$ <p style="text-align: center;">Γ is the gamma function</p>	shape parameter = α scale parameter = β
2	GEV	$F(x) = \exp\{-\exp(-y)\}$ $y = \kappa^{-1} \log\{1 - \kappa(x - \xi)/\alpha\}$	shape parameter = κ scale parameter = α location parameter = ξ
3	GLO	$f(x) = \frac{1}{\{1 + \exp(-y)\}^2}$ $y = -\kappa^{-1} \log\{1 - k(x - \xi)/\alpha\}$	shape parameter = κ scale parameter = α location parameter = ξ
4	GNO	$F(x) = \varphi(y)$ $y = -\kappa^{-1} \log\{1 - k(x - \xi)/\alpha\}$	shape parameter = κ scale parameter = α location parameter = ξ
5	GPA	$F(x) = 1 - \exp(-y)$ $y = -k^{-1} \log\left\{1 - \frac{k(x - \xi)}{\alpha}\right\}$	shape parameter = κ scale parameter = α location parameter = ξ
6	GUM	$F(x) = \exp[-\exp\{-(x - \xi)/\alpha\}]$	scale parameter = α location parameter = ξ
7	P3	$F(x) = \frac{ x - \xi ^{\alpha-1} \exp(- x - \xi /\beta)}{\beta^{\alpha} \Gamma(\alpha)}$ <p>If $\gamma \neq 0$, then let $\alpha = \frac{4}{\gamma^2}$, $\beta = \frac{1}{2} \sigma \gamma$,</p> <p style="text-align: center;">and $\xi = \mu - 2\sigma/\gamma$</p>	scale parameter = σ shape parameter = γ location parameter = μ

Note. Modified from Rizwan et al. (2018).

The major challenge in flood forecasting using the statistical distribution models is the selection of the relevant probability distribution (Rizwan et al., 2018). Furthermore, researchers recommend the user selection of a distribution, which works best for a specific site after a trial of multiple probability distribution curves (Rizwan et al., 2018; Xiong et al., 2018). In the recent past, some commonly applied PDs entail generalized extreme value (GEV), Pearson type III (P3), log Pearson type III (LP3), generalized Pareto (GPA), generalized logistic (GLO), generalized normal (GNO), exponential (EXP), gamma (GAM), Weibull (WEI), and Gumbel (GUM) (Vivekanandan, 2015).

Some countries have adopted specific standard PD for flood frequency analysis. For instance, the United States of America uses log Pearson type III (Stedinger & Griffis, 2008). China adopted Pearson type III, and Europe prefers generalized extreme value distribution (Rizwan et al., 2018). Therefore, a lack of global and regional standard probability distribution models has restrained hydrologists from using a generic distribution globally. The procedure of identifying the most reliable probability distribution model requires a goodness-of-fit test since various flood characteristics in different rivers and the availability of a wide range of selection criteria demand the selection of PDs from a wide range of available distribution.

The general framework for estimating flood magnitude, which accounts for climate variability and land-use change effects is shown in Figure 2.4.

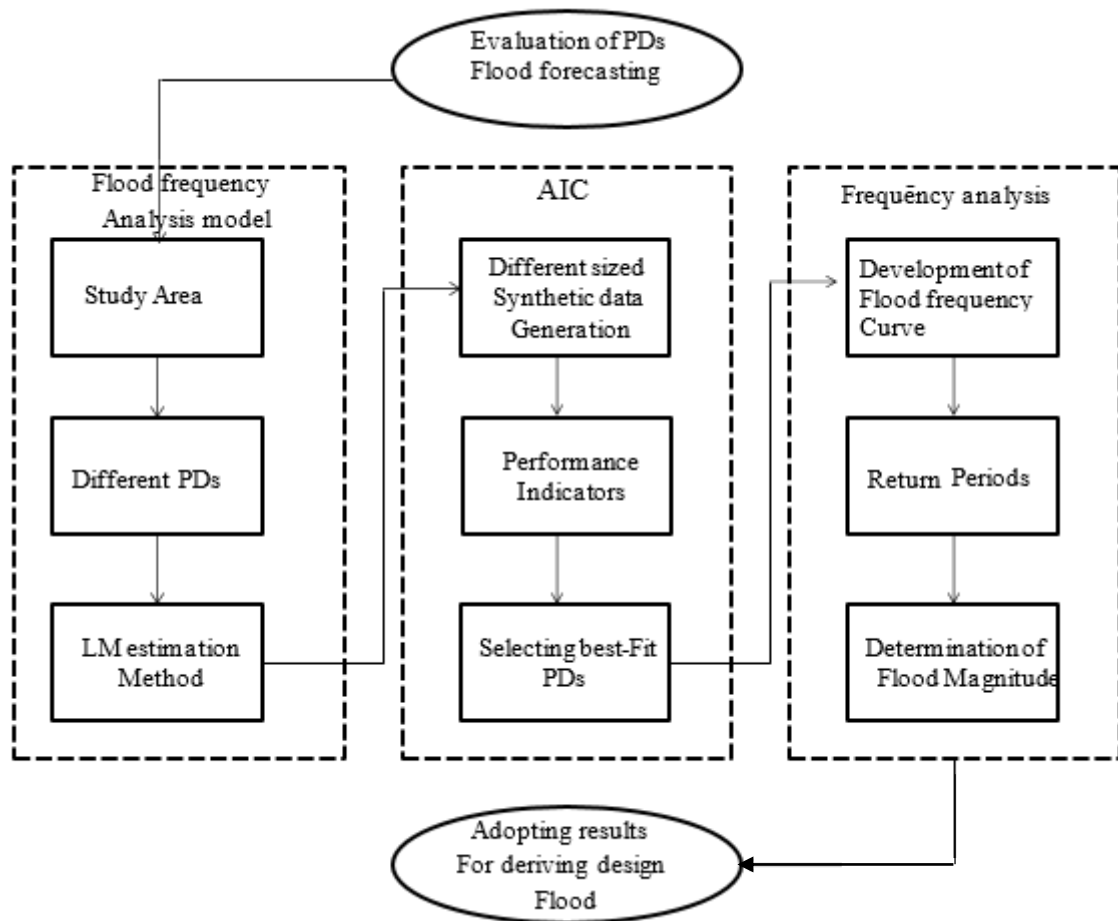


Figure 2.4: Flowchart of the procedure for flood magnitude estimation using the PDFs

While existing literature extensively discusses the methodologies and applications of flood frequency and probability distribution models, there are key areas that require further exploration. Many studies do not adequately address how the performance of these models varies across different geographic settings. This is crucial as factors such as climate,

topography, and land use significantly impact flood behavior and model accuracy. The dependency of these models on high-quality input data is often understated. In regions where data is sparse or of poor quality, the reliability of flood predictions can be severely compromised.

The potential benefits of integrating flood frequency models with other hydrological or climate models are not fully explored. Such integrations could enhance predictive capabilities and provide a more comprehensive understanding of flood dynamics. The reviewed literature provides a solid foundation for understanding flood frequency and probability distribution models. However, Future research should focus on the gaps highlighted above to enhance reliability and applicability.

2.4 Forecasting of Flood Events

The first activity in flood forecasting is the use of models or statistical tools to predict future flood magnitudes or peak discharges. Then the relevant PD curve selected was used for estimation of frequencies of the forecasted flood magnitudes. Although many techniques have been proposed and applied to predict hydrologic events, artificial neural networks have been preferred and most used (Das & Ghosh, 2018). ANN models may be a better option because of their power of adaptive learning, real-time operation, and fault tolerance, and they are used in modelling nonlinear and complex phenomena (Lee & Tuan, 2016; Ozoegwu, 2019; Somvanshi et al., 2006). Their capability comes from pattern capturing and statistical parallel processing of historical data (Ozoegwu, 2019).

Artificial neural network models have been widely applied in hydrological studies including flood predictions (Mitra et al., 2016; Mukerji et al., 2009; Rezaeianzadeh et al., 2014; Tiwari & Chatterjee, 2010;). These studies have indicated that ANN models perform better than other statistical modelling techniques because of their robust performance in dealing with noisy input patterns, and the ability to generalize from the input data, which make them a reliable option for probability predictions.

2.4.1 Artificial Neural Network

An artificial neural network can be described as a mathematical structure capable of representing the arbitrary, complex, and non-linear process correlating the input and output of any system. The motivation for the development of neural network technology stemmed from the desire to develop an artificial system that could perform "intelligent" tasks similar to those performed by the human brain (Herreyre et al., 2023; Wambua, 2020).

ANN is a black box-type lumped model, which obtains knowledge through a pragmatic approach, which involves identifying a set of weights for the connections and boundary values referred to as biases, for the neurons (Sharghi et al., 2018; Wambua, 2019). Figure 2.5 shows typical artificial nodes with inputs (X_1, X_2, \dots, X_n) connected to neuron j with weights ($W_{1j}, W_{2j}, \dots, W_{nj}$) on each connection.

The neurons sum all the signals they receive, with each signal being multiplied by its associated weights on the connection. ANN output (Q) is then processed through an activation function $f(\cdot)$, which is usually non-linear to give the final output (Y).

As explained by Barua (2010), the input and output signal relationship within the neural networks can be expressed as expressed in the following function:

$$Y = f(Q) = f\left(\sum_i^n W_i X_i + b_k\right) \quad (2.14)$$

where, X_i is the input signal i , W_i is the weight attached to the input signal i , n is the number of input signals, b_k is the bias at the cell of the body, f is the activation function, and Y is the output.

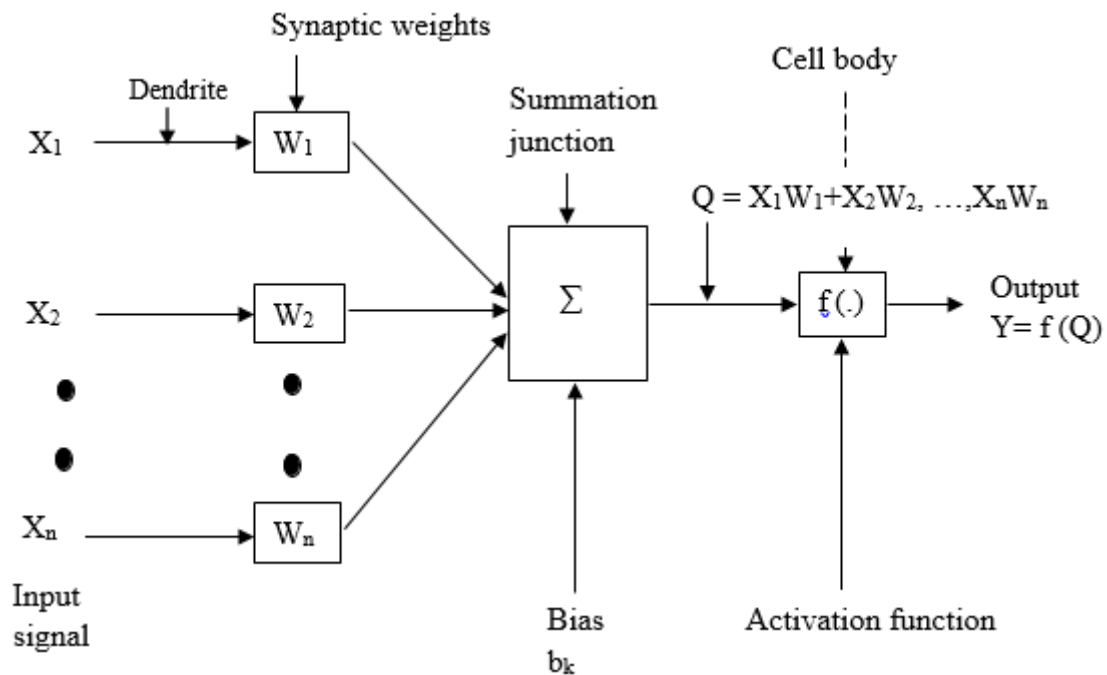


Figure 2.5: A typical Artificial Neurons Architecture

Source: Gurney, (2020).

The neurons are arranged in layers and are the components, which maps input to output. Weight (w) is part of what determines how a network behaves. Neural network knowledge is stored

within interneuron connection strengths known as synaptic weights. The activation function used in ANN is dependent on the type, learning algorithm (Levenberg-Marquardt, Bayesian Regularization, BFGS Quasi-Newton, Gradient Descent with Momentum, and Gradient Descent), and scaling approach used. The most important (and probably most used) transfer function is the sigmoid (logistic) function because of its easily differentiable properties, which is very convenient when the back-propagation algorithm is applied (Özbay & Tezel, 2010).

Figure 2.6 shows the most common transfer (activation) functions of artificial neural networks as illustrated by Bennett et al. (2013) and Mishra and Desai (2006).

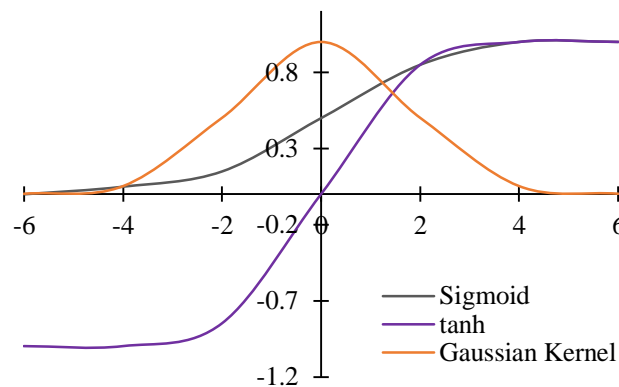


Figure 2.6: Types of Artificial Neural Network activation (transfer) functions

Artificial neural network models may be classified into feed-forward networks and recurrent neurons (Mishra & Desai, 2006). The recurrent network contains loops because of the feedback connections and they include neural network time series applications for future scenario predictions. Unlike recurrent neuron networks, the feed-forward networks have neurons organized into layers having unidirectional connections, thus characterized by neither cycles nor loops in the network. They are used in pattern recognition, curve fitting, forecasting, classifications, and data clustering. Feed-forward neural networks have been applied widely in solving real and complex hydrologic problems with great accuracy specifically the feedforward backpropagation models (Kuok et al., 2010; Peng et al., 2017).

2.4.2 Coupling ANN with the Probability Distribution Models

Flood forecasting is normally done by the use of statistical probability distribution curves that encompass the prediction of recurrence interval corresponding to specific magnitude (Rizwan et al., 2018). The best probability distribution curve is selected from the existing statistical distributions such as Gumbel, Normal, Log-normal, Exponential, Weibull, Pearson, and Log-Pearson. These graphs are then used to estimate the design flow values corresponding to

specific return periods, which can be used for hydrologic planning purposes. Therefore, relevant PD curves can then be applied to estimate the P-percent annual exceedance probability of the flood magnitudes predicted by artificial neural networks. The option of coupling models in hydrology has been observed to improve prediction efficiency (Chen et al., 2011; Guo et al., 2021; Khashei et al., 2010).

CHAPTER THREE

MATERIALS AND METHODS

3.1 The Study Area

The Gucha-Migori River Basin is an extensive basin cutting across five counties in Kenya namely, Narok, Homabay, Migori, Nyamira, and Kisii. It is located between longitudes $34^{\circ} 7' 48.08''$ E and $35^{\circ} 1' 36.6''$ E and latitudes $0^{\circ} 21' 27.09''$ S and $0^{\circ} 32' 59.24''$ S and has a total length of 147 km (Figure 3.1).

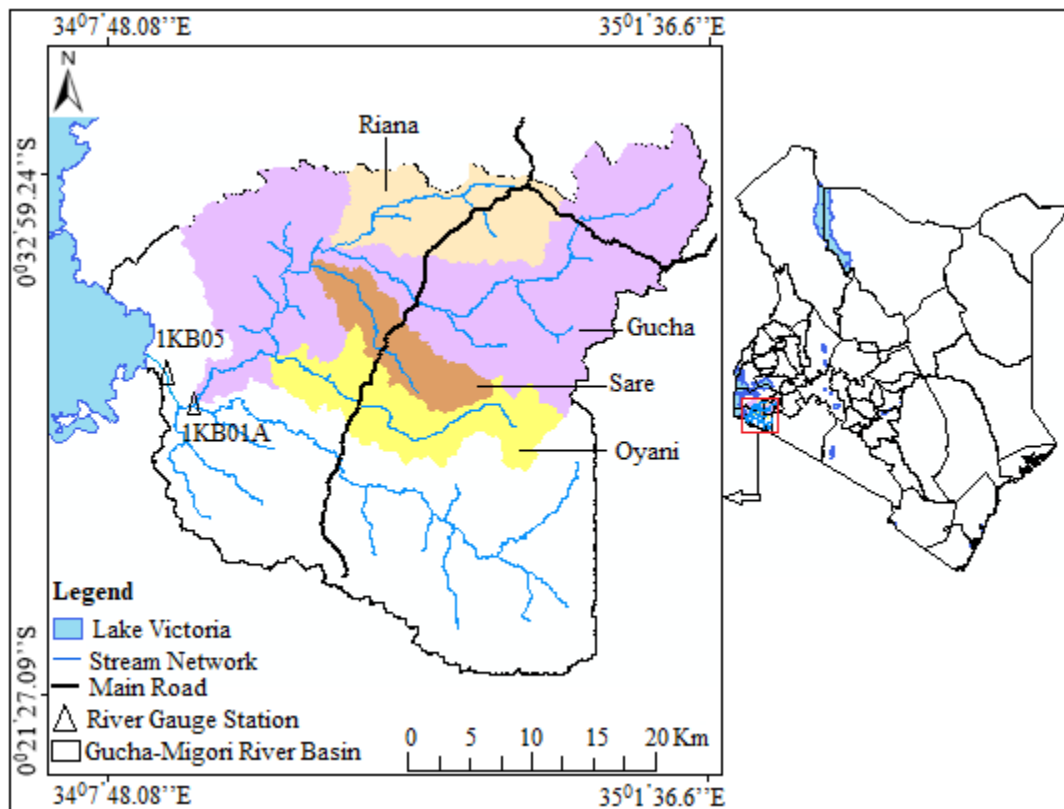


Figure 3.1: Gucha-Migori River Basin

Gucha-Migori River Basin consists of a two-river system, which is R. Gucha and R. Migori. These two rivers merge at a confluence in the Sango area in Central Kadem Location in Nyatike district to become the wide R. Gucha-Migori. The river thereafter flows and pours its water into Lake Victoria. The basin is average 2000 m above sea level but 3000 m above sea level at its source in Nyamira. R. Gucha has its source in Nyamira County in the Kisii highlands while R. Migori has its source in Narok County specifically in the Emuria Dikiri district. The climate in the Gucha River catchment is influenced to some extent by the south-easterly and north-easterly monsoon and can be classified as a modified equatorial climate. Gucha-Migori River Basin experiences two rainy seasons with the highest rainfall being between March and May.

The highlands area has rainfall of up to 2000 mm, while the lower Gucha region's rainfall is as low as 700 mm annually. Temperatures range from 15 °C to 20 °C within the highlands of Nyamira and 21 °C to 30 °C in the lowlands towards Lake Victoria. There are three River Gauging Station in the catchment; 1KB07, 1KB05, and 1KB01A. Sloping system of the basin is divided into three major categories i.e. upstream slope system of 25 % to over 40 % slope, midstream slope system of 10 % to 20 % slope, and downstream slope system of 0 % to 10 % slope. Kisii and Nyamira highlands consist of reddish fertile volcanic loamy soils while the downstream of the South Nyanza region consists of greyish fertile alluvial soils (Ogembo, 2018).

3.1.1 Spatial Data Collection

The satellite data and other geospatial data products that were downloaded and used for hydrologic modelling using the HEC-HMS model are presented in Table 3.1.

Table 3.1: Satellite remote sensing and Geospatial data products

Data	Feature values & Source
Digital Elevation Model	Earth Explorer website (https://earthexplorer.usgs.gov/). The 30 m spatial resolution (SRTM - DEM)
Soil	Food and Agriculture Organisation (FAO) data
Landsat imagery (1976) Scene size (185 x 185 Km)	Earth Explorer website (https://earthexplorer.usgs.gov/). Satellite (L1-5), Sensor (MSS), Grid cell size reflective (60 m), Map projection level – 1 (UTM), Datum (WGS 84), WRS Path/WRS row (181/60). For raster MTL.text 4Bands (Green, Red, Near Infrared 1, Infrared 2)

3.1.2 Climate Variables, Hydrologic, and Field Data Acquisition

The following data were obtained from the Water Resources Authority and the fieldwork:

- i) Daily historical meteorological data: Precipitation, mean daily surface air temperatures (from 1969 to 2015) (Figure 3B, APPENDIX B).
- ii) Daily historical hydrologic data: River discharge and water level data (from 1969 to 2015) (Figures 1B & 2B, APPENDIX B).

- iii) Coordinates of streams, reach, and the location of river gauging stations using Global Positioning System (GPS) at different points.
- iv) Coordinates of different land-use systems for supervised and unsupervised classification.

3.2 Modelling Response of River Discharge to Precipitation Variability

3.2.1 Precipitation Variability

The study began with an assessment of seasonal precipitation anomalies (January to March (JFM), April to June (AMJ), July to September (JAS), and October to December (OND)) in the Gucha-Migori River Basin spanning the years 1969 to 2015. Precipitation anomalies were computed using Equation 3.1, following established climatological methods (Coelho et al., 2012; Raible et al., 2003; WMO, 2011).

$$\text{Anomaly} = X - \bar{X} \quad (3.1)$$

where, X is actual annual value of a climate variable, and \bar{X} is the long-term average value of the variable (30~40 years).

3.2.2 Modelling of River Discharge Using HEC-HMS

Hydrologic modeling of flood events was conducted using the HEC-HMS model, chosen for its superior physical basis compared to other lumped models (Ismail et al., 2022; Natarajan & Radhakrishnan, 2020). The aim was to simulate the response of river discharge to precipitation variability, making the HEC-HMS model particularly relevant. The methodology involved preparing input data encompassing geospatial, hydrologic, and meteorological data. Subsequently, multiple model runs were conducted to compute runoff, base flow, and channel flow. Parametrization, calibration, validation, and model performance assessment were then performed to simulate and analyze flood events effectively.

3.2.3 Processing of Digital Elevation Model Data

The digital elevation model (DEM) processing was implemented using HEC-GeoHMS and the ArcMap platform. The Shuttle Radar Topography Mission (SRTM) DEM with a spatial resolution of 30 meters was clipped and projected onto Universal Transverse Mercator (UTM) based on the WGS 84/UTM zone 36S (Figure 4B, APPENDIX B).

Using the arc hydro and GeoHMS tools, morphometric and topological characteristics of the basin that were derived entail stream network, sub-basin boundaries, flow direction, flow accumulation, and outlets (Figure 5B, APPENDIX B) (Table 5A, APPENDIX A). The

derivation of the aforementioned attributes was accomplished by the use of standard procedures based on the D8 (eight-pour-point) algorithm as further explained by Olang and Fürst (2011).

The digital elevation model was crucial for accurately modeling hydrological processes within the Gucha-Migori River Basin. It provided the foundational datasets necessary for delineating watershed boundaries and stream networks, which was integral for flood modeling. The DEM processing facilitated the identification of critical basin attributes, enabling a more precise analysis of flood dynamics and potential intervention points.

3.2.4 Processing of Soil Data and Land Use - Land Cover Maps Datasets

In this study, soil data obtained from FAO was also clipped to cover the Gucha-Migori River Basin, then projected to WGS 84/UTM zone 36s, and finally rasterized in ArcMap applications (Figure 6B, APPENDIX B). The soil dataset was used to derive the major hydrological soil groups (HSG) with the help of the FAO/UNESCO revised manual for soil maps of the world as demonstrated by Batjes and Gicheru (2004).

The obtained satellite imagery of 1976 was clipped, resampled, and projected (WGS 84/UTM zone 36s) to cover the Gucha-Migori River Basin (Figure 7B, APPENDIX B).

The process of classifying land use and land cover involved using satellite imagery obtained from the Landsat 1 MSS sensor, which had four channels, including two infrared and two visible channels (Table 1A, 2A, & 3A, APPENDIX A; Figure 8B, APPENDIX B). The downloaded satellite images underwent initial pre-processing steps, such as clipping and resampling. Subsequently, they were projected to the WGS 84/UTM zone 36S coordinate system. Following this, various procedures were carried out in ArcMap version 10.4 to achieve supervised classification for the land cover, as illustrated in Figure 3.3.

These procedures included layer stacking, sub-setting, geometric correction, and ground-truthing activities as detailed in Table 4A, APPENDIX A), image enhancement, and Maximum Likelihood classification. The ground truthing of satellite imagery obtained from the Landsat 1 MSS sensor was conducted to validate the accuracy of LULC classification. Representative sample locations were selected across the study area to cover diverse and major land cover types still existing from 1976, including forest, water bodies, agricultural land, and settlements. Further references were made to the existing literature on LULC in the Gucha-Migori River Basin, such as the analysis by Muiruri et al. (2014) and Ogembo (2018), along with field

observations. GPS devices were used to record the coordinates of each location, and the land cover type was documented, supported by photographs.

The collected data was imported into GIS software and overlaid on the Landsat imagery for comparison with the classified land cover. A confusion matrix was generated to assess classification accuracy, calculating metrics such as overall accuracy, producer's accuracy, and user's accuracy. Discrepancies between the field data and the classified imagery addressed by refining the classification method and training classes. This procedure ensured the LULC classification aligned with actual ground conditions. The LULC categories that were classified included Cropland/Natural Vegetation, Tree Cover, Settlement/Bare Land, and Water.

3.2.5 Preparation of Hydrologic and Meteorological Datasets

Simulation of flood routing processes using the HEC-HMS model used daily precipitation and discharge datasets. Besides flood events simulation, river discharge datasets were also used for model calibration and validation, thus, a comparison was done between the acquired precipitation and runoff data by use of graphical plots for the test of uncertainties in the recordings. The daily precipitation and discharge data records for the period 1969 to 2015 were prepared in a Notepad as required for HEC-HMS applications and as guided by the HEC-HMS manual and other related studies (Halwatura & Najim, 2013; Nyaupane et al., 2018).

3.2.6 HEC-HMS Set-up and Run

The whole process of river discharge simulation in this study using HEC-GeoHMS and HEC-HMS is presented in a flow chart (Figure 3.6). For the simulation, the Natural Resource Conservation Service-Curve Number (NRCS-CN) model, Clark's Unit Hydrograph model, Exponential recession base flow model, and Muskingum-Cunge flow routing model were used. As explained by Doan (2000), the model elements for the basin were derived using Geo-HMS, a GIS extension to support the HEC-HMS. The Soil Conservation Service-Curve Number as expressed in Equation 3.2 was used to model the transformation of precipitation excess into direct surface runoff.

$$Q = \frac{(P - I_a)^2}{(P - I_a) + S} \quad (3.2)$$

where, P is the total precipitation (mm), Q is the actual Runoff (mm), S is the potential maximum retention of soil moisture after surface runoff begins and I_a is the initial abstraction (mm) which represents all losses before the runoff begins.

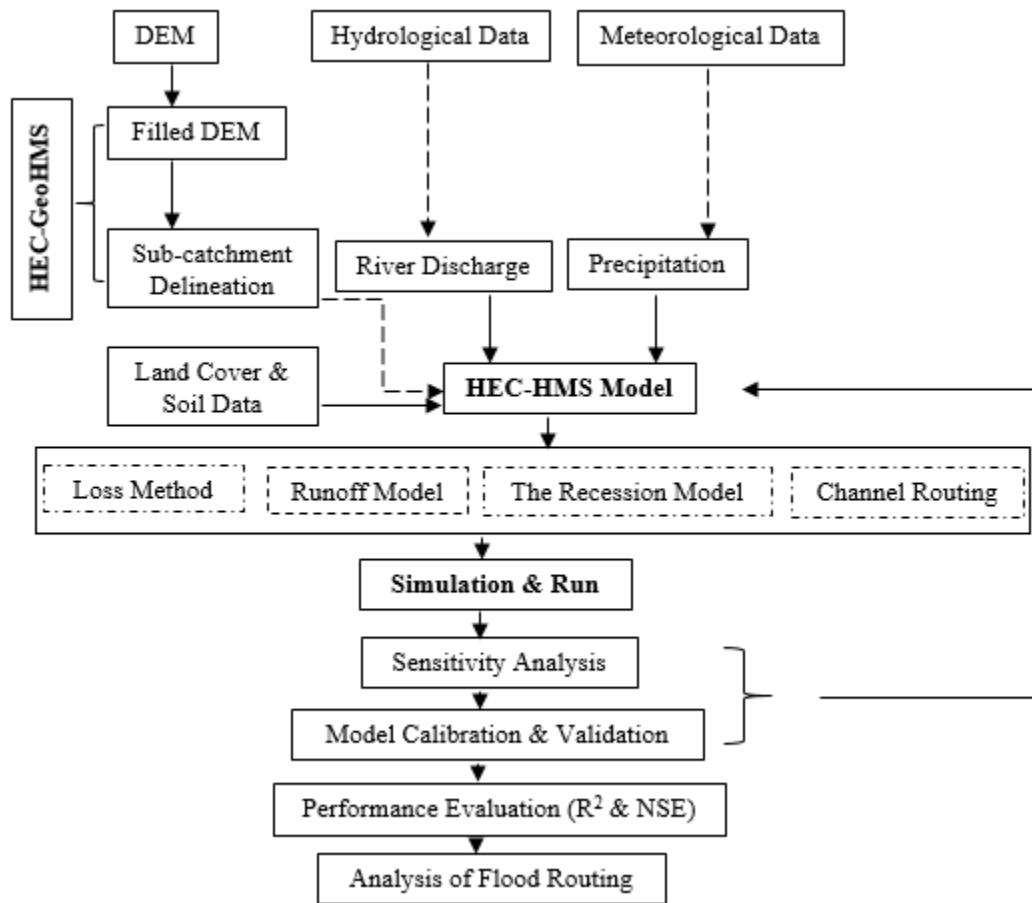


Figure 3.2: The Flow chart showing Modelling of Flood Routing by HEC-HMS

The Curve Number and potential maximum retention of soil moisture after surface runoff begins (S) are related by;

$$S = \frac{1000}{CN} - 10 \quad (3.3)$$

SCS-CN approximates runoff volumes using the physically-based dimensionless curve number (CN) parameter, which will be derived from the LULC and soil maps. Thus, CN was defined such that; and represents impervious and water surface curve numbers, and represents natural surface curve numbers. A lookup table for retrieving CN approximation was created for normal antecedent moisture conditions (AMC II) with the help of standard tables as a guide pointed out by Olang and Fürst (2011). The assumptions for initial abstractions of the maximum potential retention of the soil assumptions were carried out according to the recommendations by Doan (2000). Practical recommendations for future research and water resource management have been provided. These include specific areas for further investigation and actionable advice for policymakers to improve flood management and mitigation strategies.

Transformation of the generated runoffs into corresponding hydrographs was achieved using Clark's Unit Hydrograph concept. The application of Clark's UH requires the determination of the times of concentration (Equation 3.4) and the storage coefficient. These parameters were established from the physical catchment conditions based on procedures for the lag time (Equation 3.5) and storage coefficient.

$$T_c = KL^{0.77}S^{-0.385} \quad (3.4)$$

where, T_c is the time of concentration (day), S is the mean slope of the main river (m/m), K is 0.0078, and L is the length of main river (m).

Basin lag time can be given as:

$$t_{lag} = \frac{1}{1900Y^{0.5}} \left(L^{0.8} \times \left(\frac{1000}{CN} - 10 + 1 \right)^{0.7} \right) \quad (3.5)$$

where, L is the flow length (m), CN is the average curve number, and Y is the average slope gradient (%) of the basin.

The exponential recession model was applied to represent base flow processes. A similar approach outlined by Olang and Fürst (2011) was used to estimate the recession constant based on the relative sizes of the sub-catchments. The relationship between base flow Q_t at any time t to an initial value Q_0 , where, k is an exponential recession constant can be expressed as follows (De Silva et al., 2014):

$$Q_t = Q_0 k^t \quad (3.6)$$

Flood and channel flow routing was performed using the Muskingum–Cunge hydrologic approach (Fleming, 2004). The Muskingum-Cunge equation adopted for this study is presented in Equation (3.7).

$$Q_2 = C_0 I_2 + C_1 I_1 + C_2 Q_1 \quad (3.7)$$

$$C_0 = \frac{0.5\Delta t - Kx}{0.5\Delta t + K - Kx} \quad (3.8a)$$

$$C_1 = \frac{0.5\Delta t + Kx}{0.5\Delta t + K - Kx} \quad (3.8b)$$

$$C_2 = \frac{-0.5\Delta t + K - Kx}{0.5\Delta t + K - Kx} \quad (3.8c)$$

where, K is the time for the flood wave to pass through the river, x is the flow-specific gravity factor, the value range is 0 to 0.5, and I_1 and I_2 are the initial and final flow rates of the upper section of the river channel. Q_1 and Q_2 are the initial and final flow rates of the lower section of the river channel.

3.2.7 HEC-HMS Model Sensitivity Analysis

After the trial runs, sensitivity analyses of the parameters were based on the influence of initial loss abstraction (Ia), lag time (t_{lag}), recession constant (k), flood travel time (K), and Muskingum weighting factor (X) on the peak river discharge. The aforementioned models as illustrated in Equation 3.2, 3.4, 3.6, and 3.7 were also selected for uncertainty analysis, validation, and calibration as per the Du et al. (2012) outline. Sensitivity analysis was a fundamental component of HEC-HMS calibration that enhanced the identification of influential parameters. Each of the optimized parameters was used as an input into the model to obtain the desired simulation. The most sensitive parameters of the model needed to be precisely estimated because a minor change in the value led to a significant variation in the simulated output. The methodology for addressing uncertainty, sensitivity, calibration, and validation has been detailed. Specific techniques used, parameters tested, and evaluation criteria are explained to ensure robustness and reliability of the model.

For the accomplishment of sensitivity analysis, the model was first run using the optimized model parameters obtained after calibration and validation. Then, a one-parameter-at-a-time approach was applied, where the value of each parameter was varied from -25% to +25% in increments of 10%, while keeping all other parameters constant. The output values, particularly the river discharge data, peak flows, and base flows, were analyzed to determine variations with respect to the initial estimates of the parameters. The elasticity ratio, as expressed in Equation 3.9, was used to rank the parameters, where a greater ratio indicates a more highly sensitive variable, and a lower ratio reveals a less sensitive variable.

$$e_e = \frac{\Delta O / O_t}{\Delta I / I_p} = \frac{\% \text{ change}_{\text{output}}}{\% \text{ change}_{\text{input}}} \quad (3.9)$$

where, O and I are the input and output variables respectively.

3.2.8 HEC-HMS Model Calibration and Validation

HEC-HMS model calibration was to find the best set of parameter values that produce the best fit between simulated and observed values. The calibration and validation of the HEC-HMS

model were conducted with a split sample procedure and discharge measured records collected at the outlet of the basin (1KB05). Calibration and validation of the HMS-HEC model were achieved between the periods (January 1990 and June 1992) and (July 1992 and August 1994) respectively. The model was calibrated both manually and HEC-HMS auto-calibration process because the manual process only provides the range of the parameters while the auto-calibration process optimizes the results (Thu et al., 2019).

3.2.9 HEC-HMS Model Performance Assessment

The model performance was evaluated using two test statistics in the HEC-HMS model. The first one is the Coefficient of Determination (R^2) while the second one is Nash Sutcliffe model efficiency (Nash) and are expressed in equations (3.10) and (3.11) respectively. The performance assessment was carried out as per the guidelines, outlines, and recommendations provided by Fernandez et al. (2005) and Moriasi et al. (2007). Practical recommendations for future research and water resource management have been provided. These include specific areas for further investigation and actionable advice for policymakers to improve flood management and mitigation strategies.

$$R^2 = \frac{\left[\sum_{i=1}^n (q_i^{obs} - q_i^{avg})(Q_i^{sim} - Q_i^{avg}) \right]^2}{\sum_{i=1}^n (q_i^{obs} - q_i^{avg})^2 \sum_{i=1}^n (Q_i^{sim} - Q_i^{avg})^2} \quad (3.10)$$

$$Nash = 1 - \frac{\sum_{i=1}^n (q_i^{obs} - Q_i^{sim})^2}{\sum_{i=1}^n (q_i^{obs} - Q_i^{sim})^2} \quad (3.11)$$

where, n is the total number of observations, q_i^{obs} is the observed discharge (m^3/s), q_i^{avg} is the average of the observed data, Q_i^{sim} is the simulated discharge, and Q_i^{avg} is the average of the simulated data.

3.2.10 Discharge Hydrometric Indices and Precipitation Variability Correlation

The correlation between simulated river discharge and precipitation was done by regression analysis. Regression analysis was applied to relate the response of a quantitative dependent variable (seasonal discharges (JFM, AMJ, JAS, and OND)) to a quantitative independent variable (precipitation) in an equation form or model.

The general regression model is given as:

$$Q_1 = a_0 + a_1 h_1 + \varepsilon \quad (3.12)$$

where, Q_1 is the dependent variable, a_0 and a_1 are regression constants, h_1 is the independent variable, and ε is the average value of the random error.

Using the method of least squares, regression constants (a_0 and a_1), in such a way that the sum of squares of the residuals is minimal.

$$SSE = \sum_{i=1}^n e_i^2 = \sum_{i=1}^n (Q_1 - a_0 - a_1 h_1)^2 \quad (3.13)$$

Differentiating SSE with respect to a_0 and a_1 to obtain:

$$\frac{\partial(SSE)}{\partial a_0} = -2 \sum_{i=1}^n (Q_1 - a_0 - a_1 h_1) \quad (3.14)$$

$$\frac{\partial(SSE)}{\partial a_1} = -2 \sum_{i=1}^n (Q_1 - a_0 - a_1 h_1) h_1 \quad (3.15)$$

Setting the partial derivatives equal to zero and rearranging the terms to obtain the following normal equations:

$$n a_0 + a_1 \sum_{i=1}^n h_1 = \sum_{i=1}^n Q_1 \quad (3.16)$$

$$a_0 \sum_{i=1}^n h_1 + a_1 \sum_{i=1}^n h_1^2 = \sum_{i=1}^n h_1 Q_1 \quad (3.17)$$

$$a_0 = \frac{\sum_{i=1}^n Q_1 - a_1 \sum_{i=1}^n h_1}{n} \quad (3.18)$$

$$a_0 = \bar{Q}_1 - a_1 \bar{h}_1 \quad (3.19)$$

$$a_1 = \frac{n \sum_{i=1}^n h_i Q_i - \left(\sum_{i=1}^n h_i \right) \left(\sum_{i=1}^n Q_i \right)}{n \sum_{i=1}^n h_i^2 - \left(\sum_{i=1}^n h_i \right)^2} \quad (3.20)$$

Using the following notations:

$$S_{hh} = \sum_{i=1}^n (h_1 - \bar{h}_1)^2 = \sum_{i=1}^n h_i^2 - \frac{1}{n} \left(\sum_{i=1}^n h_i \right)^2 \quad (3.21)$$

$$S_{QQ} = \sum_{i=1}^n (Q_1 - \bar{Q}_1)^2 = \sum_{i=1}^n Q_i^2 - \frac{1}{n} \left(\sum_{i=1}^n Q_i \right)^2 \quad (3.22)$$

$$S_{hQ} = \sum_{i=1}^n (h_i - \bar{h}_1)(Q_i - \bar{Q}_1) = \sum_{i=1}^n h_i Q_i - \frac{1}{n} \left(\sum_{i=1}^n h_i \right) \left(\sum_{i=1}^n Q_i \right) \quad (3.23)$$

$$\text{Then; } a_1 = \frac{S_{hQ}}{S_{hh}} \quad (3.24)$$

For the model or the developed equation, the correlation coefficient (R) was then calculated as;

$$R = \frac{S_{hQ}}{(S_{hh}S_{QQ})^{\frac{1}{2}}} \quad (3.25)$$

Computation of inferences related to linear regression and correlation. The errors for a_0 and a_1 , in the simple linear regression, was then be determined as:

$$S_{a_0} = S_{\varepsilon} \left(\frac{\sum h_i^2}{nS_{hh}} \right)^{\frac{1}{2}} \quad (3.26)$$

$$S_{a_1} = \frac{S_{\varepsilon}}{(S_{hh})^{\frac{1}{2}}} \quad (3.27)$$

Sum of squares for error (SSE) was also calculated as:

$$SSE = S_{QQ} - a_1 S_{hQ} \quad (3.28)$$

In addition, the mean squares for error:

$$MSE = S_{\varepsilon}^2 = \frac{SSE}{df_{\varepsilon}} \quad (3.29)$$

Confidence intervals for a_0 and a_1 , is given by:

$$CI_{a_0} = a_0 \pm t_{\alpha/2, df_{\varepsilon}} S_{\varepsilon} \left(\frac{\sum h_i^2}{nS_{hh}} \right)^{\frac{1}{2}} \quad (3.30)$$

$$CI_{a_1} = a_1 \pm t_{\alpha/2, df_{\varepsilon}} \frac{MSE}{(S_{hh})^{\frac{1}{2}}} \quad (3.31)$$

Choosing the level of statistical significance at 95% ($\alpha = 0.05$), the hypothesis testing was carried out about a_0 and a_1 , using t-distribution statistical test. The rejection criterion for the null hypothesis (H_0) was when the calculated t-value (t_{cal}) is equal to, or greater than the critical t-value (t_{crit}).

$$t_{cal} = \frac{a_0}{S_\varepsilon} \left(\frac{nS_{hh}}{\sum h_1^2} \right)^{\frac{1}{2}} \quad (3.32)$$

The computation of reference durations was based on the standardized index of annual simulated river discharge, which is a robust integrator of the water balance at the basin scale. It is a method that provides the deviation from a long-term average and can translated into extreme hydrological events when the index is greater than +0.5 or -0.5, following Balme et al. (2006) criteria and illustrations. The hydrometric index was computed for hydrological seasons (JFM, AMJ, JAS, and OND) for the period between 1969 and 2015 (Equation 3.33).

$$SHI = \frac{RD_s - \overline{RD}_s}{\sigma} \quad (3.33)$$

where, RD_s is the average discharge for the season, and \overline{RD}_s is the long-term interannual mean

3.3 Developing the Relationship between Flood Magnitude and Frequency

3.3.1 Flood Frequency Analysis

Observed river discharge data was used to analyse the temporal variation of independent flood events from 1969 to 2015. Then, the next procedure was the ranking of flood magnitudes from the biggest to the tiniest event. After ranking had been achieved, return periods or recurrence intervals (frequencies) were calculated using Equation 3.34 as outlined by other studies like Bhagat (2017), Hamed and Rao (2019), and Mujumdar and Kumar (2012).

$$T = \frac{(n+1)}{r} \quad (3.34)$$

where, T is the return period, n is the number of years in record, and r is the rank of a particular magnitude of an event.

To estimate the P-percent Annual Exceedance Probability (AEP) for the flood events in the Gucha-Migori River Basin, the formula described by Olson et al. (2014) was applied (Equation, 3.35).

$$AEP = \left(\frac{1}{T} \right) \times 100 \quad (3.35)$$

3.3.2 Modelling Using Probability Distribution Models

For this study, the relationship between flood magnitudes and their respective frequencies was achieved by probability distribution function modelling. Therefore, the whole process was based on the testing of various PD curves and then the selection of the relevant model that provides a better relationship between flood magnitudes and their respective frequencies. The four tested PDMs include Normal Distribution, Log-Normal Distribution, Gumbel Distribution, and Log-person Type III Distribution.

The normal cumulative distribution function applied can be expressed as:

$$X_{N,T} = \bar{X} + K_{N,T}S \quad (3.36)$$

where, $X_{N,T}$ is the predicted discharge, at return period T, \bar{X} is the average annual peak discharge, $K_{N,T}$ is the normal deviation (Z) for the standard normal curve, where area = 0.50 – (1/T), and S is the standard deviation, of annual peak discharge.

The lognormal distribution function used can be given as;

$$X_{LN,T} = \bar{X}_1 + K_{LN,T}S_1 \quad (3.37)$$

where, $X_{LN,T}$ is the logarithm of predicted discharge, at return period, \bar{X}_1 is the average of annual peak discharge logarithms, $K_{LN,T}$ is the normal deviate (Z), of logarithms for the standard normal curve, where area = 0.50 – (1/T), and S_1 is the standard deviation, of logarithms of annual peak discharge.

The following express-guided Gumbel extreme value distribution Peak discharges to be developed:

$$X_{G,T} = \bar{X} + K_{G,T}S \quad (3.38)$$

where, $X_{G,T}$ is the predicted discharge, at return period (T), \bar{X} is the average annual peak discharge, $K_{G,T}$ is a function of return period and sample size, and S is the standard deviation of annual peak discharge.

The log-Pearson type III distribution, which applies to nearly all series of natural floods was developed as guided by the expression:

$$X_{LP,T} = \bar{X} + K_{LP,T}S_1 \quad (3.39)$$

where, $X_{LP,T}$ is the logarithm of predicted discharge, at return period (T), \bar{X} is the average of annual peak discharge logarithms, $K_{LP,T}$ is a function of return period and skew coefficient, and S_1 is the standard deviation of logarithms of annual peak discharge.

The basic paramters that were calculated include the following, mean (Eq. 3.40), Standard deviation (Eq. 3.41), and Skew coefficient (Eq. 3.42).

$$\bar{X} = \frac{\sum x}{n} \quad (3.40)$$

$$S = \frac{1}{n-1} \left(\sum (X - \bar{X})^2 \right)^{0.5} \quad (3.41)$$

$$G = \frac{n \sum (X - \bar{X})^3}{(n-1)(n-2)S^3} \quad (3.42)$$

where, X is annual peak flow (m³/s) or logarithm of annual peak flow, and n is the length of dataset.

3.3.3 Selection of Probability Distribution Model

3.3.4 Coefficient of Determination (R²)

A wide range of statistics has been used to evaluate hydrologic event predictions. By far the most widely preferred statistic reported for hydrologic variables is the Coefficient of Determination (R²) (Anupam & Pani, 2020; Kia et al., 2012; Tunas et al., 2022). The R-squared statistical performance matric was applied to measure how the observed versus simulated regression line approaches an ideal match as elucidated by Deo and Şahin (2016), Fairchild et al. (2009), and Moriasi et al. (2015). R² values range from 0 to 1, with a value closer to 0 or 0 indicating no correlation. In addition, a value closer to 1 indicates relative perfect linear covariation between the two datasets (similar spatial or temporal patterns). It implies that a correlation measurement would suggest a higher accuracy of the model when the value is approaching one. Using R² (Equation 3.9), the performance assessment of the four test PDCs was rated according to Fernandez et al. (2005) and Moriasi et al. (2007) recommendations. Practical recommendations for future research and water resource management have been provided. These include specific areas for further investigation and actionable advice for policymakers to improve flood management and mitigation strategies.

3.3.5 Goodness of Fit (GoF) Test

The concept of GoF test statistics is to evaluate the performance of the probability distribution curve. It was preferred and accepted for checking the reliability of PDMs to observe river discharge or hydrologic variables datasets based on Langat et al. (2019) elaborations. It can be illustrated by χ_{rs}^2 K_s statistics as follows:

$$\chi_{rs}^2 = \sum_{f=1}^N \frac{\left(O_f(Q_f) - F_f(Q_f)\right)^2}{F_f(Q_f)} \quad (3.43)$$

where, $O_f(Q_f)$ is the observed frequency value of the j th class, N is the number of frequency classes, and $F_f(Q_f)$ represents the expected frequency value of the j th class.

$$K_s = \text{Max}_{f=1}^N \left(E_e(Q_f) - E_d(Q_f)\right) \quad (3.44)$$

where, $E_e(Q_f)$ is the empirical CDF of Q_f and $E_d(Q_f)$ is the computed CDF of Q_f as given by Langat et al. (2019). If the calculated values of the GoF test statistics were lower than those of the theoretical values at the chosen significance level, then the model distribution was taken to be acceptable for estimation. The distribution was considered acceptable for the estimation of extremal floods when the computed values of the GoF test statistics were lower than those of the theoretical values at a defined level of significance. Some of the tests that were used for the comparison of the observed and theoretical CDF are discussed below.

3.3.6 Anderson-Darling (AD) Test

This test compares an observed PDF to a theoretical PDF and gives more emphasis to the tail of the distribution in the χ_{rs}^2 statistics and thus was useful for the detection of outliers. If the AD statistics were more than a critical value of 2.5018 at a 95 % significance level ($\alpha = 0.05$), then the test hypothesis was rejected. The AD test statistics,

$$A^2 = -N - \frac{1}{N} \sum_{i=1}^N (2i-1) \times (\ln F_e(Q_f) + (\ln(1 - F_D(Q_f)))) \quad (3.45)$$

where, A^2 is the Anderson-Darling test statistics, F_e is the cumulative distribution function of the specified distribution, and Q_f is the ordered observed data.

3.3.7 Kolmogorov-Smirnov Test

The Kolmogorov-Smirnov (KS) test (Langat et al., 2019) statistics is based on the greatest vertical distance from the empirical and theoretical PDFs, and similar to the AD test statistics, the rejection of a hypothesis was done if the KS statistic was more than the critical value 0.20517 at a 95 % significance level of confidence (Equation 3.46):

$$D = \text{Max}\left(F(Q_l) - \frac{l-1}{N}, \frac{l}{N}(F(Q_l))\right) \quad (3.46)$$

where, $F(Q_l)$ is the number of points is less than Q_l , and they Q_l are ordered from the smallest to the largest value. This represents a step function that increases by $1/N$ at the value of each ordered data point. F is the theoretical cumulative distribution of the distribution being tested, which must be continuous, and it must be fully specified.

3.3.8 Cramer-Von Mises Test

This test statistic, unlike the Anderson-Darling and Kolmogorov-Smirnov tests, considers an observed hydrological time series in increasing order. The Cramer-von Mises statistic γ^2 is computed as in Equation (3.47) (Langat et al., 2019).

$$\gamma^2 = \sum_{l=1}^N \left(F(Q_l) - \frac{l-0.5}{N} \right)^2 + \frac{1}{12N} \quad (3.47)$$

If the test statistic γ^2 is more than a critical value of 0.221 at a 95 % significance level ($\alpha = 0.05$), the test hypothesis is rejected.

3.3.9 Best-Fit Distribution Curve

Firstly, classical descriptive statistics of the external data were processed, and a skewness-kurtosis plot for the empirical distribution showing values for common distribution was made to assist in the initial visualization and choice of distribution to fit the data. Firstly, goodness-of-fit (GoF) statistics were computed. The quality of fit was assessed using classical goodness-of-fit statistics (Kolmogorov-Smirnov, Cramer-von Mises, and Anderson-Darling statistics). Model estimation and selection of the best-fit distribution for the site were accomplished using information criteria (AIC) and Bayesian Information Criterion (BIC). Where both model estimation and selection could be simultaneously accomplished.

$$AIC_c = -2LL + 2k + \frac{2k(k-1)}{n-k-1} \quad (3.48)$$

$$AIC_c = n \ln \left(\frac{SSE}{n} \right) + 2k + \frac{2k(k+1)}{n-k-1} + n \ln(2\pi) + n \quad (3.49)$$

where, AIC is the information criterion, n is the number of observations, and k is the number of parameters of the probability distribution model.

$$BIC = -2LL + k \ln n \quad (3.50)$$

$$BIC = n \ln \left(\frac{SSE}{n} \right) + k \ln n + n \ln(2\pi) + 2 \quad (3.51)$$

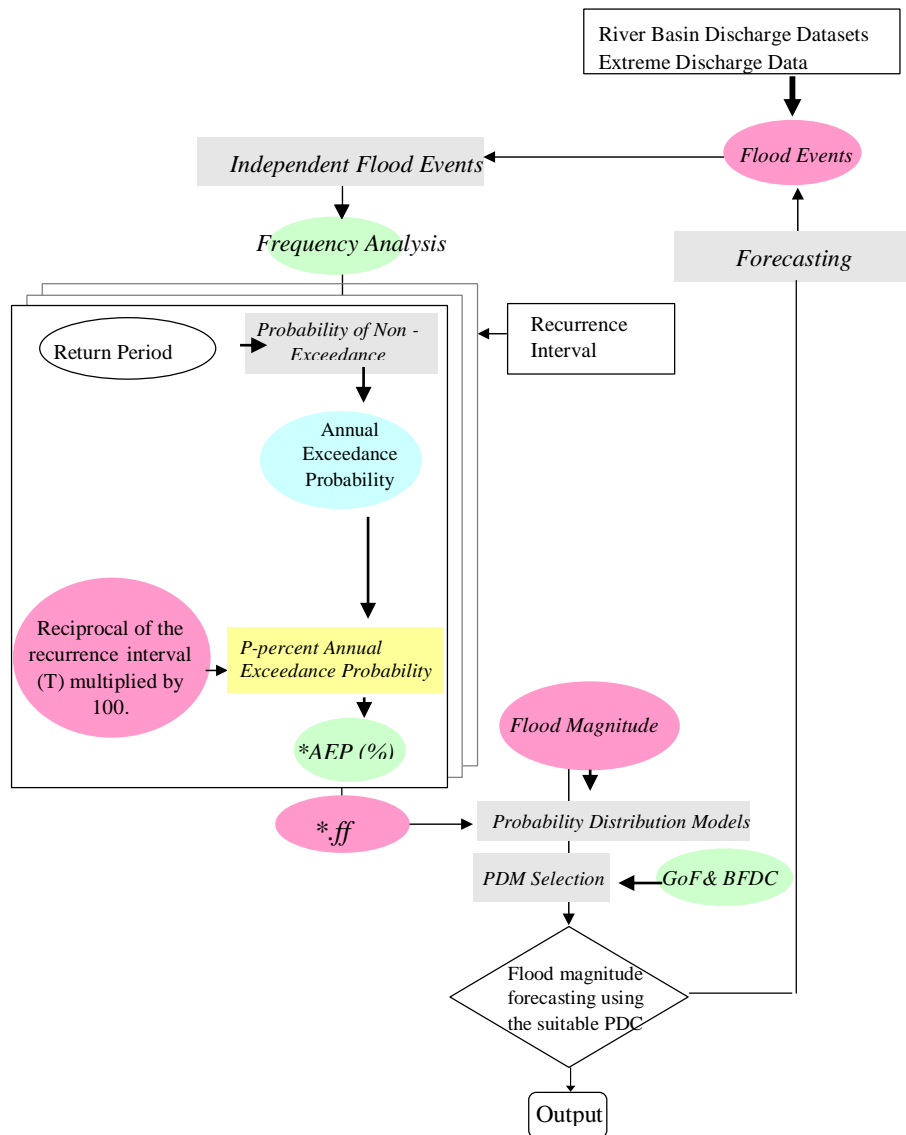
where, BIC is the Bayesian Information Criterion, and SSE is the residual sum of squares

$$SSE = \sum_{i=1}^n (\gamma_i - Y_i)^2 \quad (3.52)$$

where γ_i stands for the i -th data samples, Y_i is the estimated values from the probability distribution curves for the value of Y_i and n the upper limit of summation.

3.3.10 Estimation of Flood Magnitudes and Probability of Exceedance

The whole procedure and framework used in this evaluation are presented in Figure 3.7.



This figure shows the link between observed extreme river discharges, independent flood events, flood frequency (ff), return period, and the forecasting of the flood magnitudes. Forecasting using suitable PDF.

Figure 3.3: General schematic framework for flood magnitude forecasting

Usually, flood forecasting is done by the use of statistical probability distribution curves that encompass the prediction of recurrence interval corresponding to specific magnitude (Rizwan et al., 2018). In this study, after modelling the relationship between flood magnitude and frequency from the available data using the selected probability distribution model, the curve was then used to estimate the design flow values corresponding to specific return periods. Thus, the identified suitable PDM out of the tested four (Normal, Lognormal, Gumbel, and Log-Pearson Type III Distribution) was then applied to predict the P-percent annual exceedance probability of the flood magnitudes. Some of the periods considered for forecasting include 50,

100, and 200 years, which can provide insights to be applied for hydrologic planning purposes and flood mitigation measures.

3.4 Forecasting of Flood Events and their Respective AET

After modelling the relationship between magnitude and frequency from the available data using the selected probability distribution curve, the next procedure followed the forecasting for the period between 2015 and 2052 using NAR and PDF. A nonlinear autoregressive neural network as shown in Figure 3.8 was used for the time series forecasting of the flood magnitudes while the selected probability distribution function was used for the forecasting of the respective recurrence intervals.

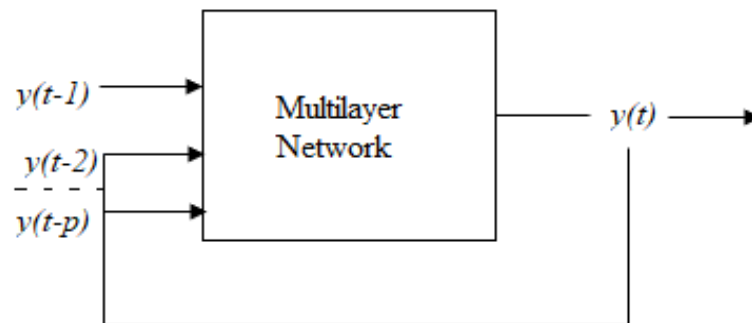


Figure 3.4: The NAR neural network for forecasting flood magnitudes

The forecasting model for flood magnitudes was developed by the past values of flood magnitudes, and this was guided by Equation (3.53). Levenberg-Marquardt backpropagation was adopted as the training algorithm because it is the most preferred learning technique for the Non-linear autoregressive neural network (Alwakeel & Shaaban, 2010).

$$(y(t)) = h(y(t-1), y(t-2), \dots, y(t-p)) + \varepsilon(t) \quad (3.53)$$

The p features $y(t-1), y(t-2), \dots, y(t-p)$, are the feedback delays

Equation (3.53) explains how NAR was applied in forecasting. The value of a data series of a given flood event (y) at time t , $y(t)$, using the p past values of the series. $h(\cdot)$ function was not known in advance. It was approximated by optimization of the network neurons and weight bias. And, $\varepsilon(t)$ represents the error of the approximation of the series y at time t . Mean Square Error was used as the objective function for synaptic weight adjustments.

$$MSE = \frac{SSE}{n} \quad (3.54)$$

$$SSE = \sum_{i=1}^n (\gamma_i - Y_i)^2 \quad (3.55)$$

where γ_i stands for the i -th data samples, Y_i is the estimated values from the network for the value of Y_i and n the number of data samples for neural network training.

Weights adjustments will be achieved as per Equation 3.56.

$$w_{ij}(n+1) = w_{ij}(n) + \Delta w_{ij}(n) \quad (3.56)$$

where, $\Delta w_{ij}(n)$ is the corresponding weight change, achieved through the jacobian matrix, identity matrix, and scalar factor.

All the modelling computations and programming of the forecasting models development, training, testing, and validation were carried out in MATLAB LaBolatory (MATLAB) version 2019 platform (e.g. Figure 10B, 11B, & 12B, APPENDIX B). The model performance of comparing the trained model predictions with the actual values was carried out by the use of statistical error indices. They include Coefficient of Determination and Mean Square Error (MSE) as described in Equations (3.10) and (3.53) respectively. Considering the daily time step forecasting for peak discharge in March, April, May, and June, the performance evaluation of the models developed was rated according to Moustiris *et al.*, (2010) recommendations. Practical recommendations for future research and water resource management have been provided. These include specific areas for further investigation and actionable advice for policymakers to improve flood management and mitigation strategies.

CHAPTER FOUR

RESULTS AND DISCUSSION

4.1 Modelling Response of River Discharge to Precipitation Variability

4.1.1 Precipitation Variability

The precipitation annual anomalies over the Gucha-Migori River Basin for January, February, and March (JFM) are presented in Figure 4.1.

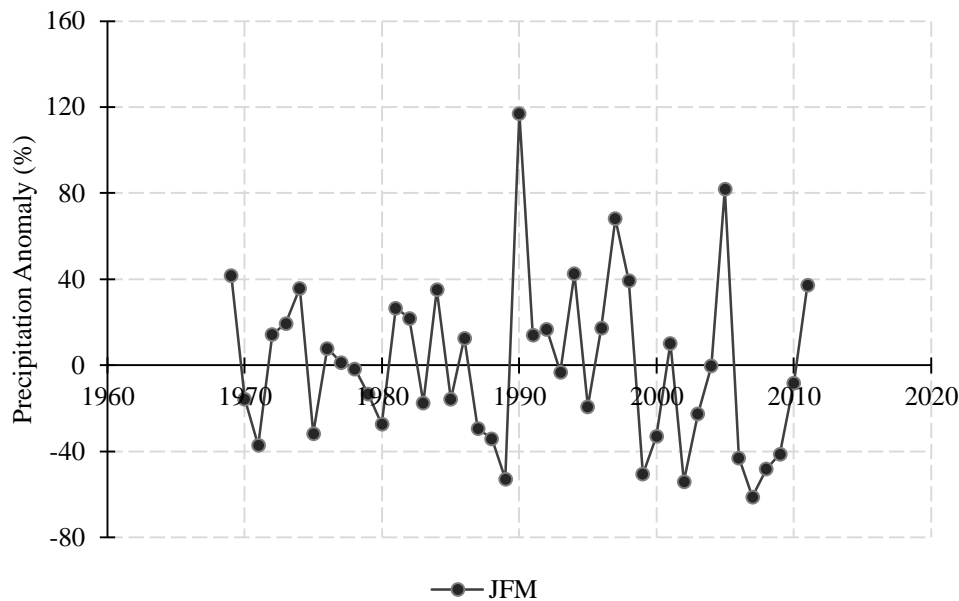


Figure 4.1: Precipitation Anomaly for the Months of January, February, and March

From the results of the average JFM precipitation datasets, the anomalies for the 43 years varied between -61.21 (2007) and 117.15 % (1990) of the long-term average. Values beyond -35 and $+35$ % anomalies threshold were considered as extremely dry and wet climatic conditions respectively. These anomaly ratings were based on the findings of IPCC (2007) and Rwigi et al. (2016) recommendations. However, the precipitation anomalies above 40 % indicated periods associated with river discharges that cause flooding events. Practical recommendations for future research and water resource management have been provided. These include specific areas for further investigation and actionable advice for policymakers to improve flood management and mitigation strategies.

Daily mean precipitation for January, February, and March ranged from 8.23 to 1.47 mm for the period between 1969 and 2015. Out of all the annually recorded precipitation events, 11.63 % (events of above +40 anomalies) represented extremely wet climatic conditions. Eight

independent flood events occurred in January (1973 and 2007), February (2007 and 2010), and four events in March (1969 and 1985) for the period between 1969 and 2015.

The precipitation annual anomalies over the Gucha-Migori River Basin for the months of April, May, and June (AMJ) are shown in Figure 4.2.

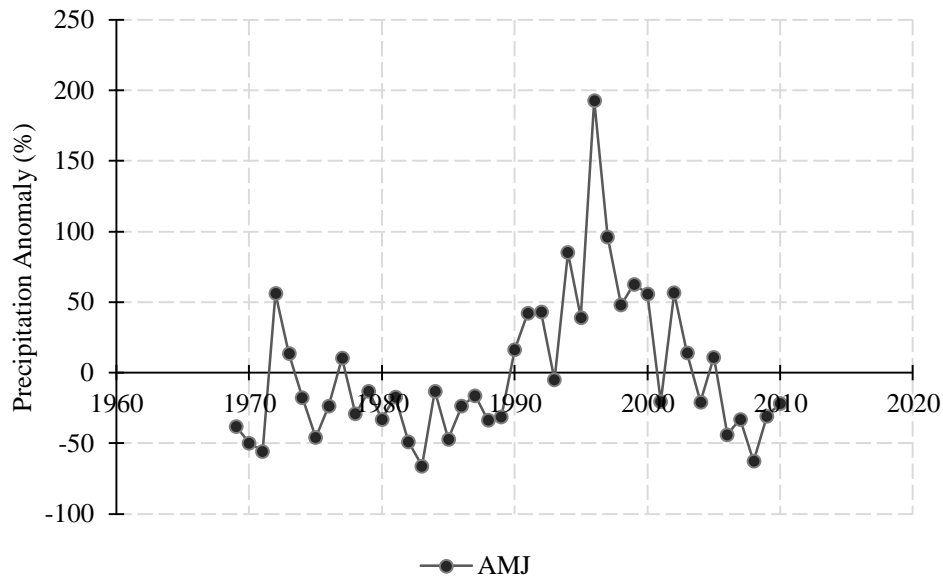


Figure 4.2: Precipitation Anomaly for the Months of April, May, and June

Based on the mean daily precipitation data of the period 1969 and 2015 for April, May, and June, the anomalies ranged between -65.97 (1983) and 192.89 % (1996) of the long-term average. The year 1983 had the lowest (1.15 mm) recorded mean daily precipitation for the three months while 1986 had the highest (9.9 mm). Out of all the annually recorded precipitation events, 23.81 % (events of above +40 anomalies) represented extremely wet climatic conditions. Independent flood events experienced in April include 1(1971), 2(1974), 1(1977), 2(1969), 2(1979), 1(1981), 1(1982), 1(1985), 1(1990), 1(2004), 1(2006), 1 (2011), and 4 (2013) in the study area.

In the case of May, the number of independent flood events recorded include one, three, five, and two occurring in the years 1977, 2012, and 2013, respectively while only 2 in June 1982. Precipitation trends in any of the periods, anomalies, and temporal variation for the months (April, May, and June) showed the manifestation of variability. The variability would affect the spatial as well as temporal response of inflow, storage, and outflow in a catchment hence changes in quantity and dynamics of stream flow (Amisi, 2021; Kundu, 2007; Mwetu, 2019; Ongoma & Chen, 2017; Rwigi, 2016).

The precipitation annual anomalies over the Gucha-Migori River Basin for July, August, and September (JAS) are presented in Figure 4.2.

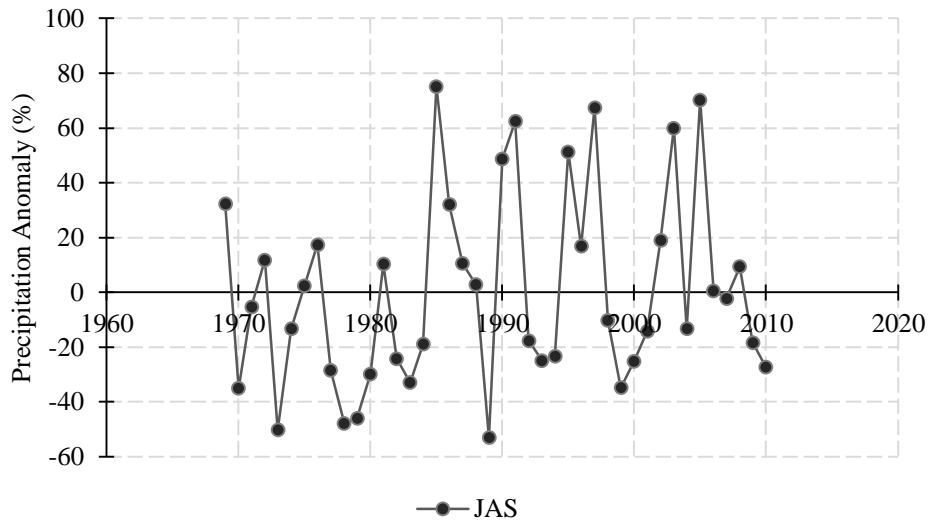


Figure 4.3: Precipitation Anomaly for the Months of July, August, and September

As indicated in Figure 4.3, the mean daily precipitation data of the period 1969 and 2013 for July, August, and September, the anomalies ranged between -53.11 (1989) and +75 % (1985) of the long-term average. The year 1989 had the lowest (1.51 mm) mean daily precipitation for the three months while 1985 had the highest (5.64 mm). Out of all the annually recorded precipitation events, 16.28 % (events of above +40 anomalies) represented wet climatic conditions. There were no independent flood events in July, August, and September for the period 1969 and 2015.

The precipitation anomalies for October, November, and December (OND) are shown in Figure 4.4.

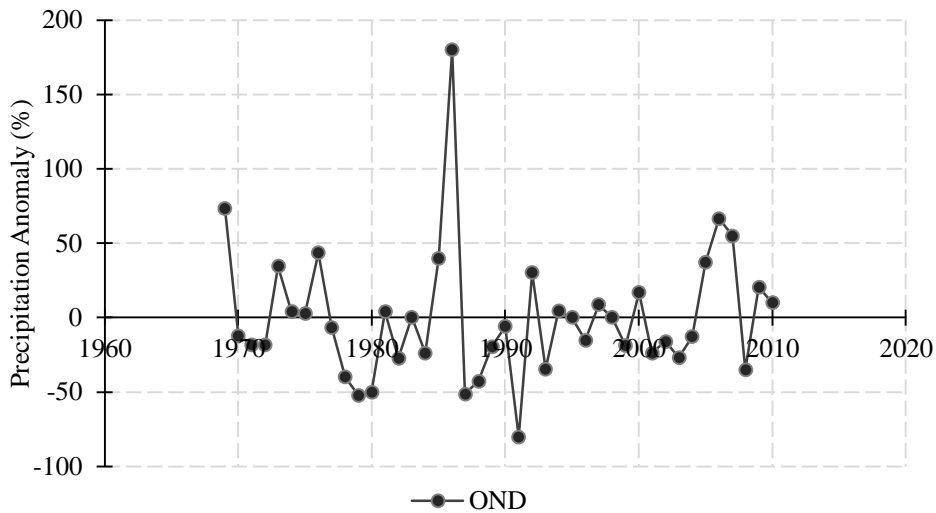


Figure 4.4: Precipitation Anomaly for the Months of October, November, and December

As revealed in Figure 4.4 of the mean daily OND precipitation datasets, the anomalies for the 43 years ranged from -80.20 (1991) and 179.87 % (1986) of the long-term average. Daily mean precipitation for October, November, and December varied from 8.34 to 0.59 mm. Out of all the yearly-recorded precipitation events, 11.63 % (events of above +40 anomalies) represented wet climatic conditions. There was no record of independent flood events in October and November. Nevertheless, six events (3 in 1982 and another 3 in 2011) occurred in December for the period between 1969 and 2015.

The monthly and seasonal precipitation variability at the Gucha-Migori River Basin could be attributed to changes in the Hadley circulation that imply a twice-a-year relocation of the Intertropical Convergence Zone (ITCZ). Dry seasons and months are associated with the effects of low-level north-easterly winds from Egypt and the Arabian Sea over equatorial East Africa in January and February (Camberlin, 2018). The characteristics exhibited by the monthly and seasonal precipitation variability from one year to another (as shown in Figures 4.1, 4.2, 4.3, and 4.4) were sufficient evidence of unreliable changing weather patterns hence the manifestation of extreme hydrologic events. It implies that some months would experience extreme (flooding) or reduced (drought) runoff, subsurface flow, recharge, and return flow, thus river discharge variation. Each figure in the Results and Discussion chapter is accompanied by a detailed explanation, describing what the figure shows, interpreting the data, and explaining its relevance to the study. Figures are well-labeled and referenced in the text.

4.1.2 Calibration and Validation of the HEC-HMS Model

Parametrization, calibration, and validation for the river discharge simulation were done at the sub-basin 1 (Figure 4.5 and Figure 4.7). The calibration range and fitted HEC-HMS model parameter values are presented in Table 4.1.

Table 4.1: Initial Parameters from HEC-GeoHMS Used in the HEC-HMS Model

Parameter Name	Range	Initial Value	Optimized Value
Land Use Curve Number	35.00~95.00	67.10	78.00
Lag Time SCS	0.02~1000.00	318.60	636.04
Muskingum X-value	0.17~0.50	0.20	0.19
Muskingum K-value	26.77~36.77	27.00	29.31
Basin Reach	1.00~14.00	1.00	2.00
SCS CN – CN ~ Scale Factor	0.01~100	1.00	0.01

Simulations were accomplished using the same values but the output hydrograph was not a relatively perfect match to that of the observed river discharges (Figures 4.5 and 4.7). Besides, the parameters' ranges (Table 4.1) represent model output, which is an envelope of relatively fair solutions from a lumped process expressed by a certain level of prediction uncertainty. Thus, the disparity could be attributed to uncertainties associated with merging the sub-basins and using the average parameters in the simulation process. The methodology for addressing uncertainty, sensitivity, calibration, and validation has been detailed. Specific techniques used, parameters tested, and evaluation criteria are explained to ensure robustness and reliability of the model. Each figure in the Results and Discussion chapter is accompanied by a detailed explanation, describing what the figure shows, interpreting the data, and explaining its relevance to the study. Figures are well-labeled and referenced in the text.

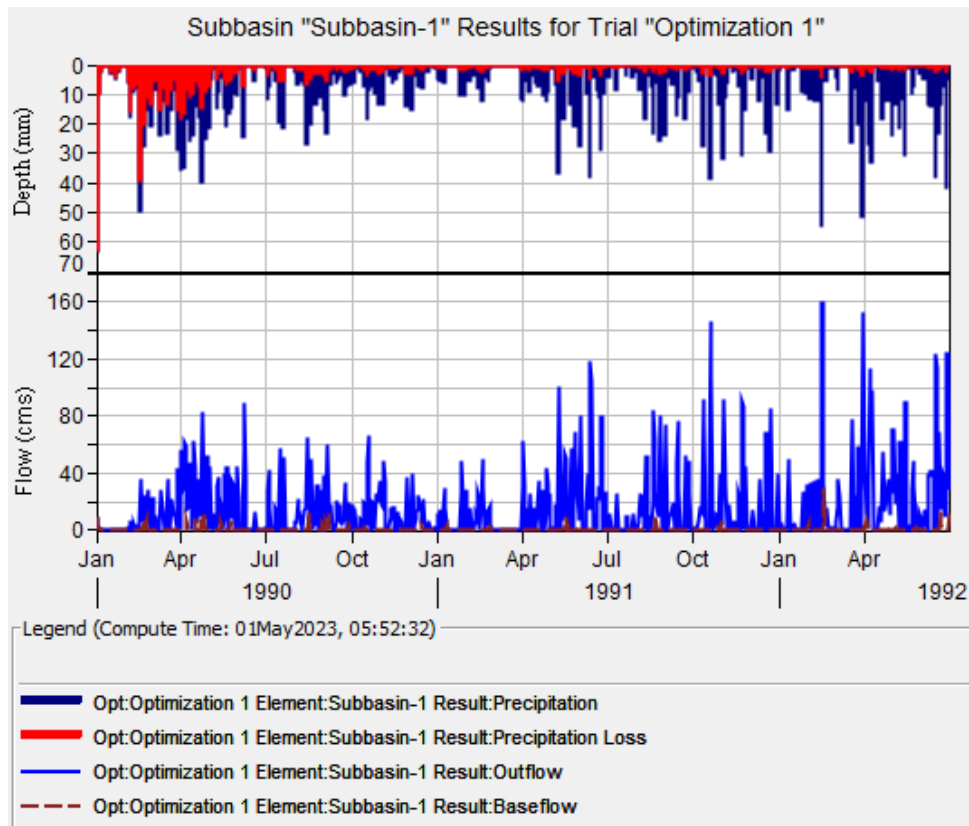


Figure 4.5: Calibration Optimization Simulation Element

For the calibration (Figure 4.6), the optimization trials of the parameterization process yielded discharge outputs that were not acceptable performance according to the recommendations by Moriasi et al. (2007) and Van Liew et al. (2003). As indicated in Figure 4.6, the R^2 and NSE values for calibration of daily river discharge at sub-basin 1 were 0.52 and 0.36 respectively. From the hydrographs, the observed values exceeded the simulated values by 9.5 %. This is a margin considered reasonable for analyzing the hydrologic modeling of the basin and not for forecasting purposes (Bajirao et al., 2021; Doherty & Johnston, 2003; Ogembo, 2018). Practical recommendations for future research and water resource management have been provided. These include specific areas for further investigation and actionable advice for policymakers to improve flood management and mitigation strategies.

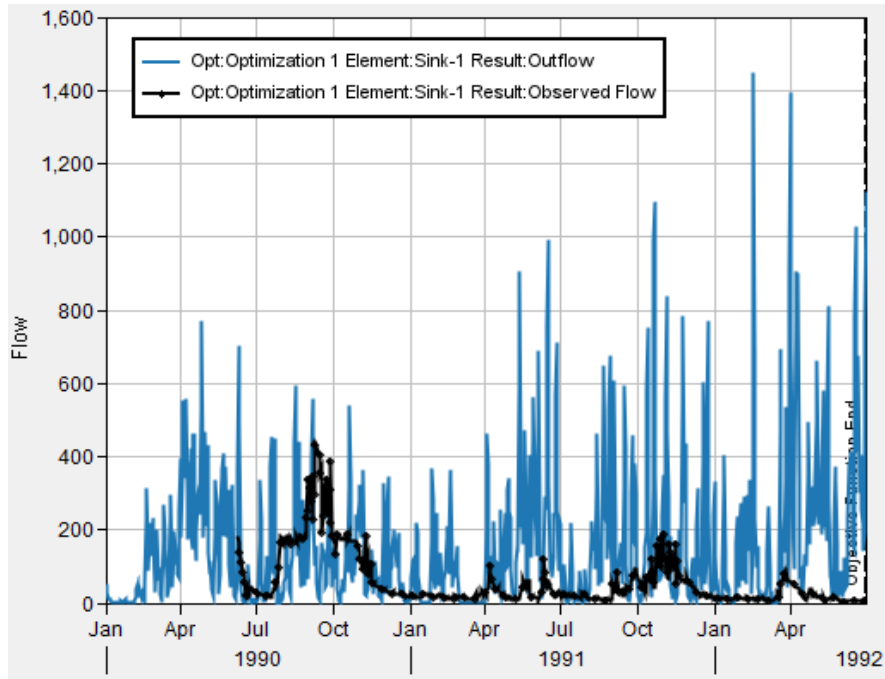


Figure 4.6: Calibration of HEC-HMS using Observed River Discharge Data at 1KB05

Figure 4.7 shows the validation trial simulations for the Gucha-Migori River Basin.

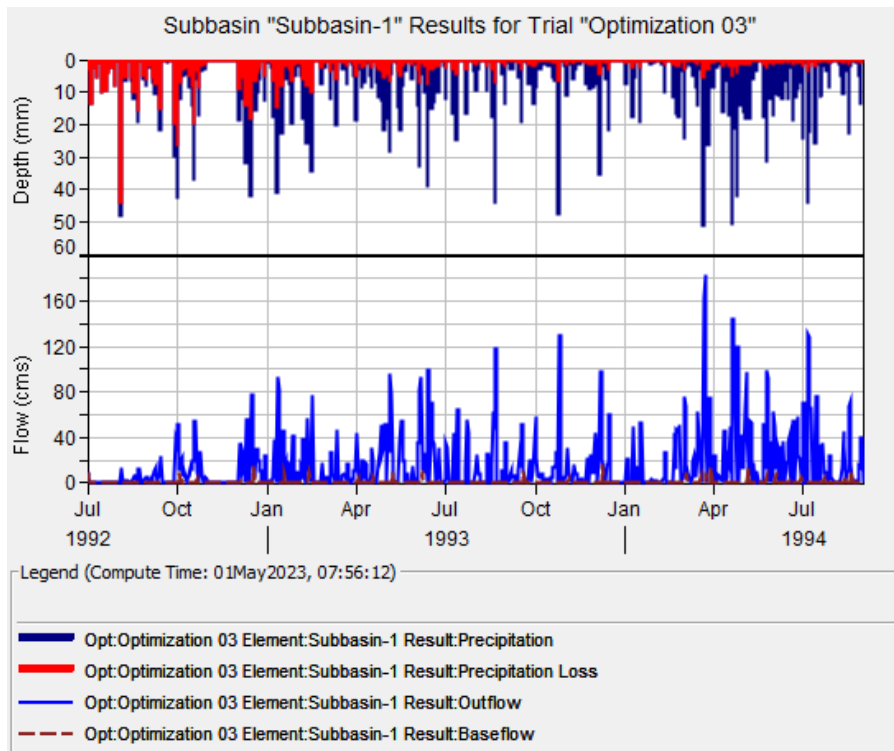


Figure 4.7: Validation Optimization Simulation Element

Simulations were accomplished using the optimized values but the output hydrograph for the validation was not the perfect match to that of the observed river discharges (Figure 4.7).

As given in Figure 4.8, R^2 and NSE values for validation of daily river discharge were 0.42 and 0.31 respectively.

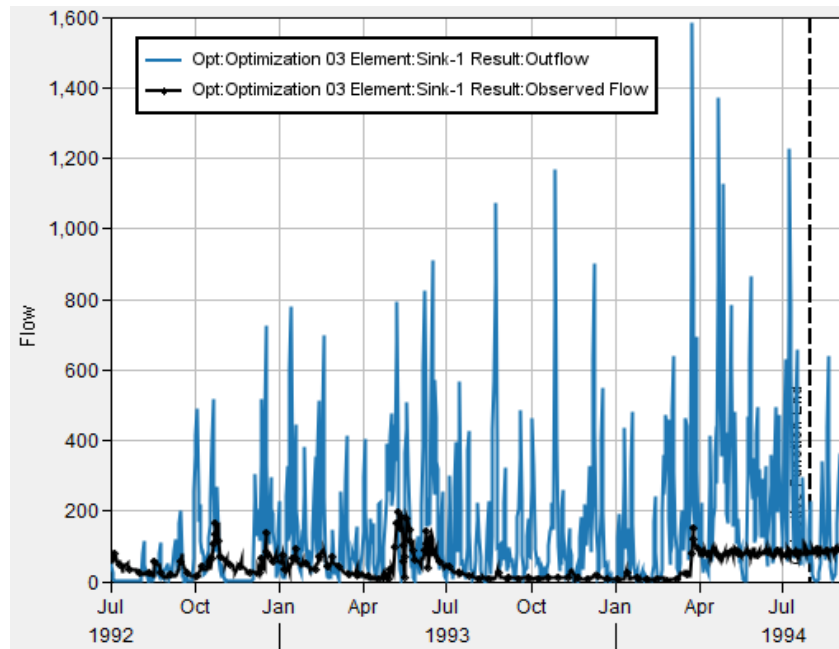


Figure 4.8: Validation of HEC-HMS using Observed River Discharge Data at 1KB05

The reduction in the coefficient of determination value from 0.52 to 0.42 could have been a result of errors in the rainfall and streamflow data due to several missing data. Another factor that could have led to this reduction may be due to the merging of 49 sub-basins to simplify the simulation process. The most likely factor for such a variation may be associated with the fact that the precipitation data did not represent the spatial variability of the entire basin. Besides, in the research carried out by Yassin et al. (2015) in Pakistan, the validation results linked to a single meteorological station were also less than the calibration results with an NSE value of 0.44. They further recommended the use of many weather station datasets to meet international standards and improve the modelling accuracy.

These results (Figures 4.6 and 4.8) are close to those attained by Hashmi (2005) when studying rainfall–runoff modelling from the Kaha hill torrent watershed in Pakistan where a difference of 8.2 % was considered acceptable. Since the difference in the observed and simulated did not exceed 10 %, these results were within the permissible limits for inference of the correlation between the precipitation and river discharge datasets. However, as had been expected, the

HEC-HMS model underestimated most of the peak flows and low flows. Other studies carried out in the same river basin with corresponding HEC-HMS performance include Ogembo (2018).

4.1.3 Correlation between River Discharge and Precipitation Variability

The Pearson correlation coefficient (two-tailed) was used to check the relationship between river discharge and precipitation as revealed in Figure 4.9.

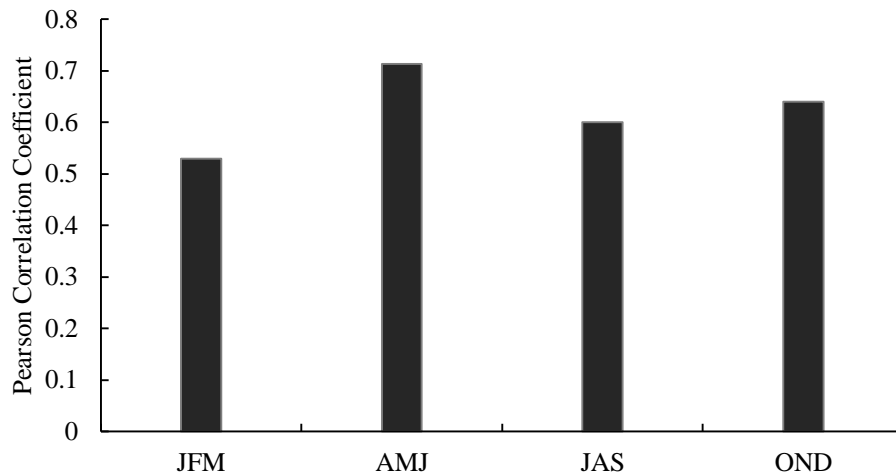


Figure 4.9: Pearson Correlation Coefficient between Precipitation and River discharge

Based on Figure 4.9, the correlation coefficients between daily averaged precipitations for JFM, AMJ, JAS, and OND and the corresponding river discharges had a significant positive correlation at the significance level of 0.05. Out of all the precipitation and simulated river discharge datasets in all the months, the strongest relationship ($r = 0.714$) was found in wetter months (April, May, and June) while the weaker correlation ($r = 0.529$) was realized in dry months (January, February, and March). In practice, it is often necessary to solve problems involving variables, which by experience are known to have an inherent relationship (Su et al., 2012; Weisberg, 2005). Thus, it can be concluded with 95 % confidence that the precipitation data is a key and useful variable for modelling spatial and temporal river discharge variability in Gucha-Migori River Basin. Other studies with corresponding results include (Stephens et al., 2015; Szolgayova et al., 2014).

Figure 4.10 represents standardized hydrometric indices for the season from January to March. The season is characterized by 18 positive and 25 negative indices. From the correlation analysis of the JFM, precipitation values could only account for 28 % of the river discharge

variance, hence, the total number of negative (wet conditions) and positive (dry conditions) indices out of the total number of the standardized hydrometric indices.

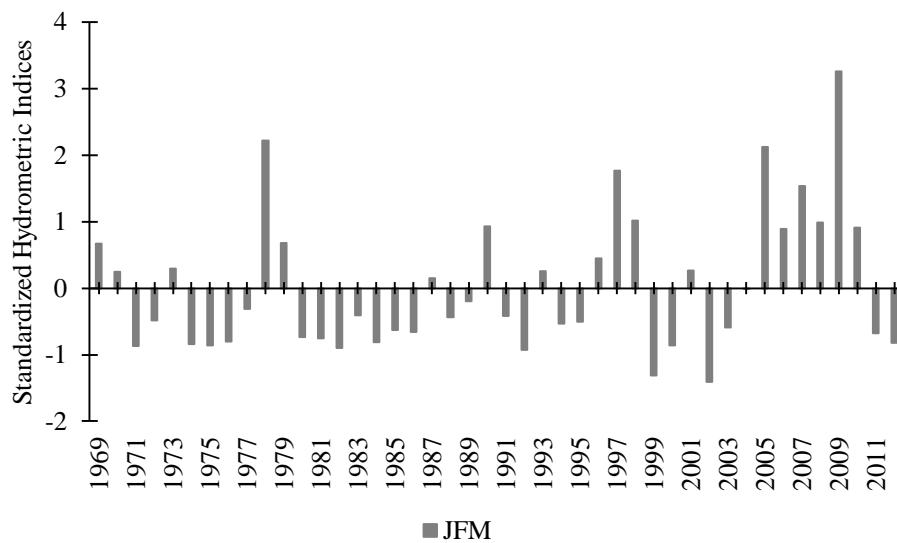


Figure 4.10: Standardized Hydrometric Indices for the January, February, and March

Figure 4.11 shows river discharge variability for the period (1969 – 2012) for the season from April to June. A total of 22 years had positive indices while 20 had negative indices. However, precipitation data could only explain 51 % of the variability or the hydrometric patterns of the simulated river discharge data for the aforementioned season.

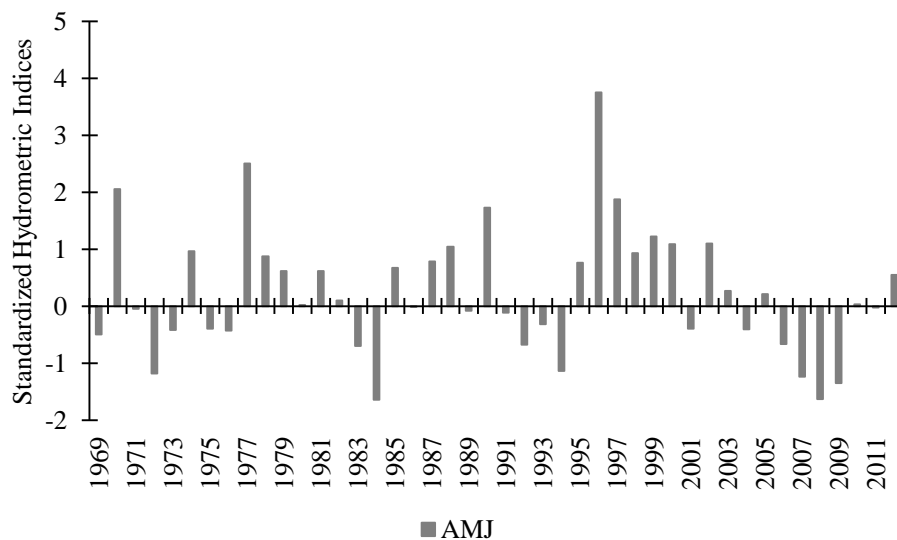


Figure 4.11: Standardized Hydrometric Indices for the April, May, and June

As indicated in Figure 4.12, 23 years had positive indices while 21 had negative indices for river discharge variability for the period (1969 – 2012) for the season from July to September.

Nevertheless, the precipitation dataset could only account for 36 % of the variance of the simulated values and variability or the hydrometric patterns of the simulated river discharge data.

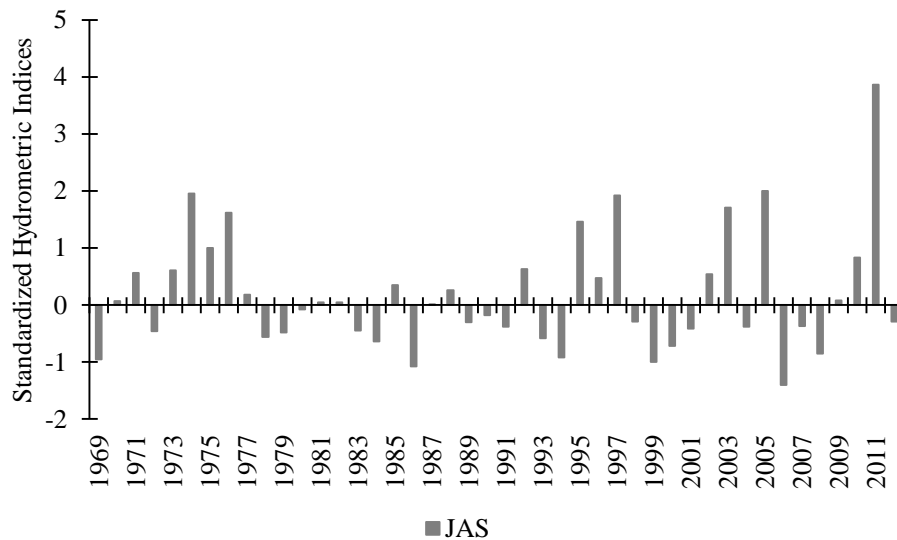


Figure 4.12: Standardized Hydrometric Indices for the July, August, and September

Figure 4.13 represents river discharge variability for the period (1969 – 2012) for the season from October to December. A total of 12 years had positive indices while 30 had negative indices.

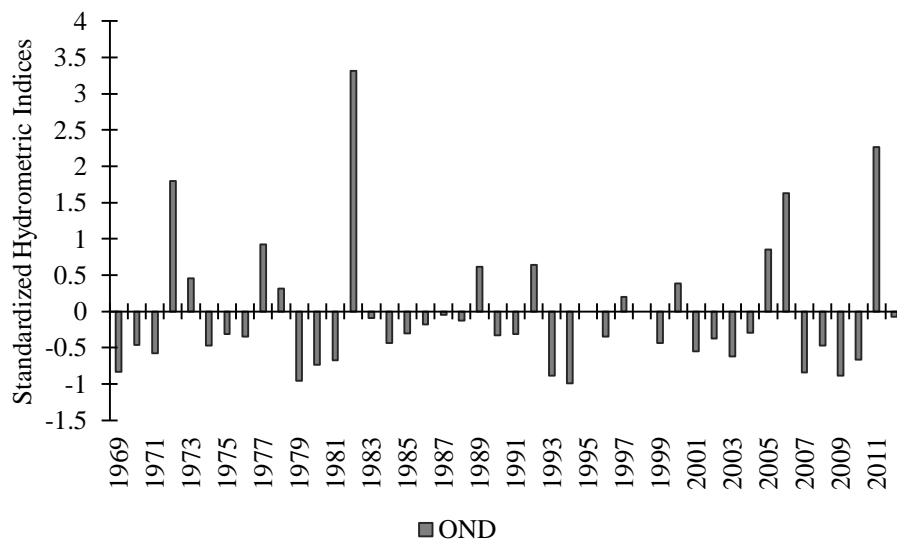


Figure 4.13: Standardized Hydrometric Indices for the October, November, and December

Nonetheless, precipitation values could only explain 41 % of the variability or the hydrometric patterns of the simulated river discharge datasets. Some of the related studies with corresponding analyses on discharge hydrometric indices entail Gao et al. (2011), Jahangir and

Nour et al. (2011), Tremblay et al. (2021), and Yarahmadi (2020). In the aforementioned studies, the +0.5 and -0.5 hydrometric indices represented extreme wet and dry climatic conditions respectively. It implies that for the case of the Gucha-Migori River Basin, flood occurrences were simulated by the HEC-HMS model in 12, 18, 13, and 8 years for the seasons JFM, AMJ, JAS, and OND respectively. There was sufficient evidence of the close relationship between precipitation variability and simulated river discharge temporal variations.

4.2 Correlation of Flood Magnitude and Frequency using PDFs

4.2.1 Flood Frequency Analysis

Figure 4.14 represents the frequency analysis of the independent floods of the Gucha-Migori River Basin.

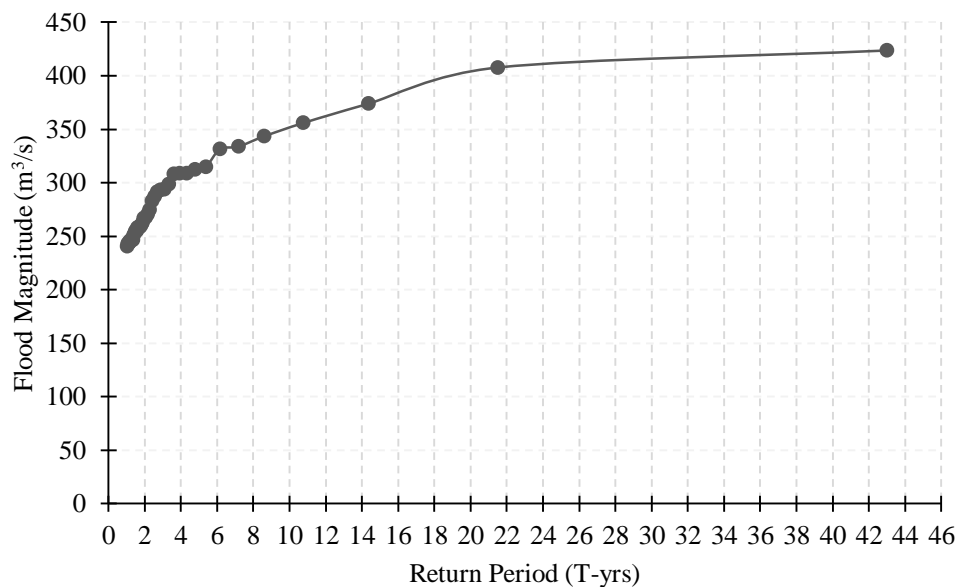


Figure 4.14: Return Period of the Independent Flood Magnitude at G-M River Basin

Out of the 132 flood events that occurred in the period 1969 to 2015, only 42 were identified as independent flood events. From the analysis, the highest and lowest, and the average and standard deviation of the recorded independent flood events were 423.90, 240.8, 284.80 m³/s, and 45.54 respectively (Figure 4.14).

Figure 4.15 presents the percent annual probability of exceedance. The probability of a flood event of a magnitude equal to or exceeding the lowest discharge (240.8 m³/s) and the highest flow (423.90 m³/s) occurring for a particular year were 0.98 and 0.02 respectively. The probability of a flood event ranging between the highest and the lowest discharge occurring was 0.96. It can be inferred that a flood event equal to or which exceeds 423.90 m³/s in the

Gucha-Migori River Basin has a 1-in-43 chance of occurring in any given year. However, a flood event of magnitude $240.8 \text{ m}^3/\text{s}$ has a 1-in-1.02 chance of occurring in any particular year. Another way of the statistical inference for Figure 4.14 and Figure 4.15 is to allude that flood events of magnitude $240.8 \text{ m}^3/\text{s}$ and $423.90 \text{ m}^3/\text{s}$ are 1-year and 43-year floods respectively. This does not mean, nevertheless, that a flood of discharge $423.90 \text{ m}^3/\text{s}$ in the G-M River Basin will only occur every 43 years. Besides, 30 or more 45-year floods may easily occur within weeks or months of each other, or the opposite could be true, where there could easily be more than 30 years between two floods of this magnitude. Similarly, Brunner et al. (2016), Salas and Obeysekera (2014), Serinaldi (2015), and Shiau (2003) have expounded on the same observation, which actually agreed with the study's results.

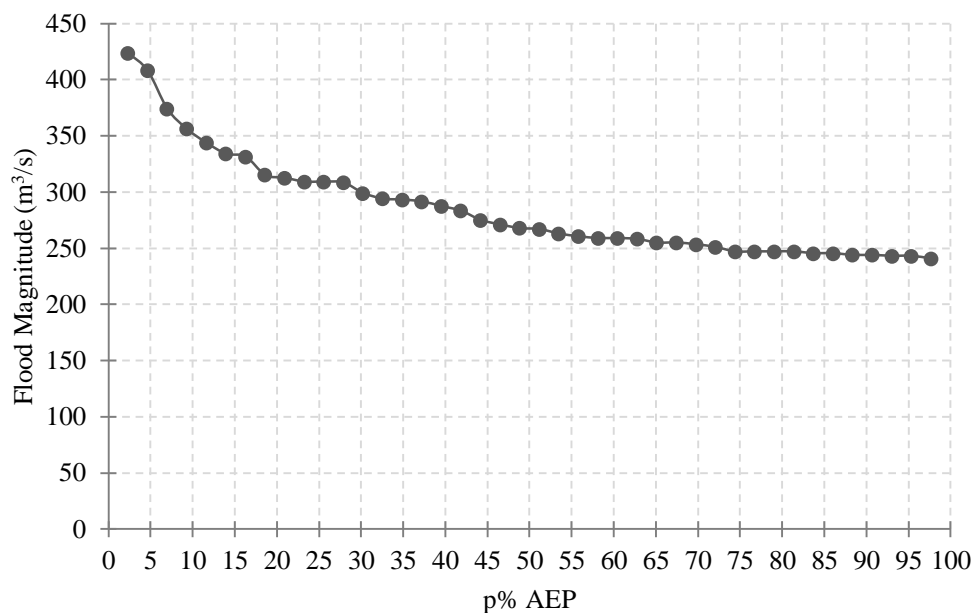


Figure 4.15: The percentage of percentage Annual Exceedance Probability

4.2.2 Performance of Probability Distribution Models

The computation of parameters for the derivation of the predicted magnitude for all floods with different return periods (1.05, 1.11, 1.25, 2, 5, 10, 25, 50, 100, and 200) are presented in Table 4.2 (log Pearson 3), Table 4.3 (Log-Normal), and Table 4.4 (Gumbel). For Log Pearson Type 3, the mean value of 2.4, standard deviation (0.064), skewness coefficient (0.0417), and location parameter ($C = 1.109$) were obtained correspondingly. The calculated mean and standard values for the normal distribution function were 284.8 and 45.54.

Table 4.2: Log Pearson 3 Parameters and Estimated Flood Magnitudes

C for Log P3	T-yrs	P	K	Y=log (Q)	Q(T-Log P3)
1.109	1.05	95.2	-1.277	2.368	233
	1.11	90.1	-1.105	2.379	239
	1.25	80	-0.848	2.395	249
	2	50	-0.181	2.438	274
	5	20	0.744	2.497	314
	10	10	1.340	2.536	343
	25	4	2.067	2.582	382
	50	2	2.588	2.616	413
	100	1	3.091	2.648	445
	200	0.5	3.582	2.679	478

C is the location parameter; K is the frequency factor; P is the probability of occurrence (%); T is the estimated flood magnitude (Theoretical).

As indicated in Table 4.3, the mean value of 2.4, standard deviation (0.064), skewness coefficient (0.0417), and location parameter (C = 0) were determined for the Log-Normal Function.

Table 4.3: Log Normal Parameters and Estimated Flood Magnitudes

C for LogN	T-yrs	Kz for LogN	Z(T-logN)	Q(T-LogN)
0	1.01	-2.326	2.250903	178.19824
0	2	0	2.4	251.18864
0	5	0.842	2.453972	284.4279
0	10	1.282	2.482176	303.51223
0	25	1.751	2.512239	325.26632
0	50	2.054	2.531661	340.14289
0	100	2.326	2.549097	354.07609
0	200	2.576	2.565122	367.38515

The mean value, reduced mean value, standard deviation, A –factor, and B-factor for the Gumbel distribution model computed were 284.8 m³/s, 0.54 m³/s, 45.54, 38.279, and 263.998 respectively.

Table 4.4: Gumbel's Parameters and Estimated Flood Magnitudes

T-yrs	P	F=1-p	Y = -ln((-lnF))	Q(T-Log P3)
1.05	95.2	0.048	-1.11	221.38
1.11	90.1	0.099	-0.84	231.92
1.25	80	0.200	-0.48	245.77
2	50	0.500	0.37	278.01
5	20	0.800	1.49	321.39
10	10	0.900	2.25	350.11
25	4	0.960	3.20	386.39
50	2	0.980	3.90	413.31
100	1	0.990	4.60	440.03
200	0.5	0.995	5.30	466.65

C is the location parameter; Y is the frequency factor; F is the probability of non-exceedance; T is the estimated flood magnitude (Theoretical).

The theoretical flood magnitudes and the corresponding recurrence intervals of the four Probability distribution functions are shown in Figure 4.16.

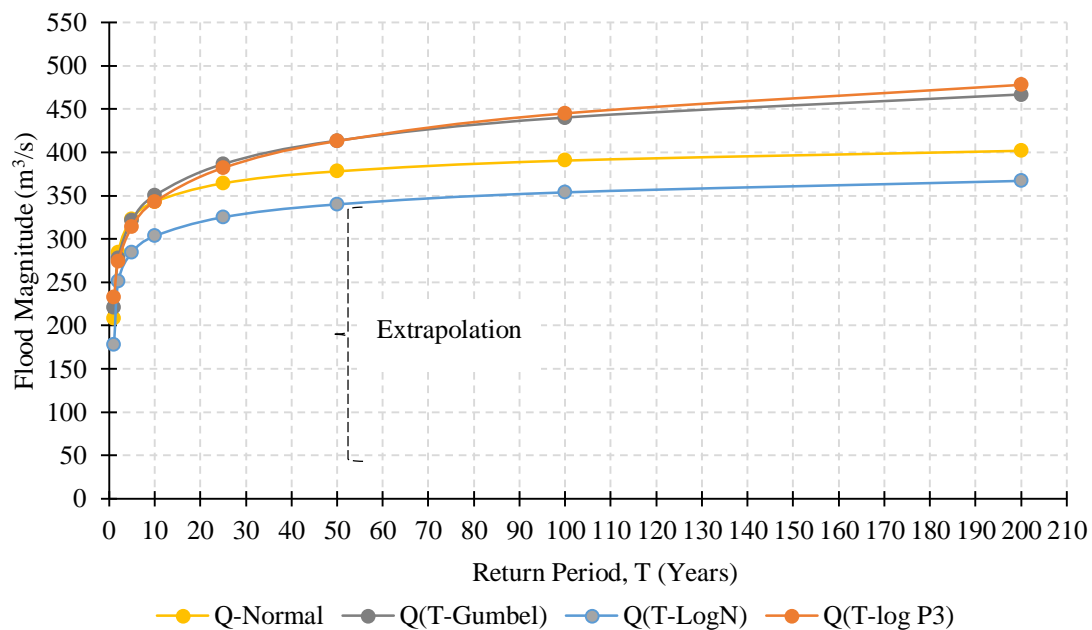


Figure 4.16: Flood Frequency Estimates by the Selected Probability Distribution Curves

Considering the predictions from Gumbel, Log P3, Log N, and Normal models, for the return periods 1.05 and 200 years, the flood magnitude estimated for G-M River Basin would be 221.38 and 466.65, 233 and 478, 178.19 and 367.38, and 209 and 402 m³/s (Figure 4.16). The

probabilities of the exceedance as predicted by the developed distribution curves are attributed to the recurrence intervals of the recorded actual independent flood events. Besides, estimated flood magnitudes from the four probability distribution curves showed a satisfactory response of peaks related to the return periods, hence, consistency with analyses in Figure 4.14.

4.2.3 Suitable Probability Distribution Curve Based on R^2

The performance comparison of the theoretical curves with the actual datasets is shown in Figure 4.17.

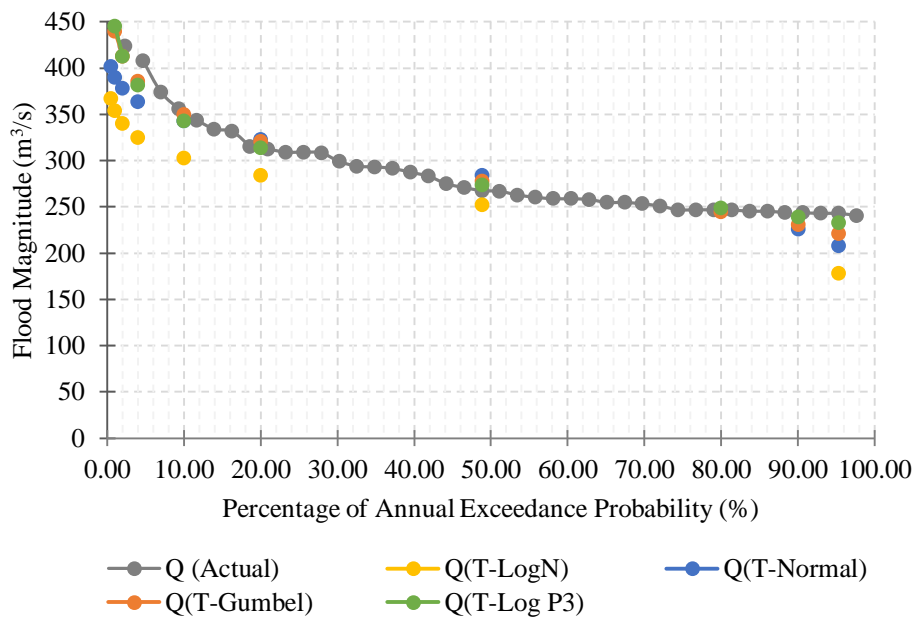


Figure 4.17: Performance comparison of the four Probability Distribution Models

Based on the coefficient of determination, the Gumbel distribution curve appeared to be the best fit of the four distribution models. It is only the Gumbel curve that accounted for at least 95 % of the variance of flood discharges, though, followed closely with the Log Pearson Type 3, which accounted for 92 %. It can then be postulated that there is a 95 % chance that Gumbel's simulated values would have a similar pattern in recurrence interval compared to the actual flood magnitude.

In comparison to Log Pearson 3, Log Normal, and Normal Distribution, the predicted flood magnitudes for the Gucha-Migori River Basin by Gumbel Probability Distribution can be considered the best alternative based on R^2 statistics. It explains why in many river basins in Kenya, the Gumbel Distribution Curve has been widely adopted for forecasting extreme hydrologic events. Example, in Narok, Kenya (Houessou-Dossou et al., 2019), Ngong River Basin (Juma et al., 2021), Nzoia Sub-basin (Ngina & Opere, 2017), Nile Equatorial Basins

(Opere et al., 2006). Additionally, it has also been widely adopted for forecasting in River Tana Basin (Maingi & Marsh, 2002), and Lake Victoria Basin (Ndetei, 2006), which is one of the neighbouring basins to the G-M River Basin.

4.2.4 GoF Statistics-Based Assessment for Suitable PDC

The Kolmogorov-Smirnov, Cramer-von Mises, and Anderson–Darling tests were used to examine the four probability distributions at a 95 % significance level ($\alpha=0.05$) (Table 4.5).

Table 4.5: Comparison of Goodness-of-fit Statistics

Probability Distribution Models	Kolmogorov-Smirnov (Critical value at 0.05 = 0.205)		Cramer-von Mises (Critical value at 0.05 = 0.221)		Anderson-Darling (Critical Value at 0.05 = 2.501)	
	Statistic	Rank	Statistic	Rank	Statistic	Rank
Gumbel	0.044	1	0.036	1	0.202	1
Normal	0.049	2	0.038	2	0.256	2
Log Normal	0.057	3	0.041	3	0.423	3
Log Pearson type 3	0.060	4	0.059	4	0.578	4

As indicated in Table 4.5, the classical goodness-of-fit test statistics for the Kolmogorov–Smirnov, Cramer–von Mises, and Anderson–Darling tests were found to be satisfactory in this context for estimating flood magnitudes based on a 95% significance level. The calculated test statistics values were lower than the theoretical values for the four chosen probability distributions at the selected significance level. Each distribution was assigned a rank from one to four, with one indicating the best fit and four indicating the poorest fit. The results of the goodness-of-fit tests pointed to the Gumbel model as the best-fitting distribution for the river discharge dataset in the Gucha-Migori River Basin.

It's worth noting that the choice of the most suitable probability distribution curve may vary from one basin to another due to temporal and spatial variations in river behavior and the uncertainties associated with model development. For instance, in the Kenyan Tana River Basin, Langat et al. (2019) identified Lognormal and gamma (Pearson type 3) distribution models as the best fits for maximum stream flows. For annual minimum flows, the Weibull, GEV, and Gumbel functions were found to be the best fits, while Lognormal functions were the best fits for annual mean flows. Similar findings were reported by other researchers,

including Norbert et al. (2014) in the Lake Victoria Basin, Kenya, and Maingi and Marsh (2020) in the context of quantifying hydrologic impacts in the Tana River, Kenya.

4.2.6 Best-Fit Distribution Curve

The model selection process employs the Akaike Information Criteria (AIC), which utilizes the same response variables across candidate distributions to compare different probability distributions. It doesn't mix null hypothesis testing with information criterion models. The best model is chosen based on the lowest calculated AIC value. Similarly, the Bayesian Information Criterion (BIC) relies on the likelihood function for model selection. Lower BIC values suggest fewer explanatory variables and a better fit. The ideal distribution is the one that best satisfies the criteria of goodness-of-fit statistics and information criterion-based model selection for extreme datasets.

In Table 4.6, you can find the results of the best-fit distribution model selection based on AIC and BIC for the extreme distribution type in the Gucha-Migori River Basin. The Gumbel and Log Pearson type 3 models were identified as the most suitable functions for representing extreme river discharges in the Gucha-Migori River basin, as they had the lowest AIC and BIC values.

Table 4.6: Best fit distribution model selection based on AIC

Probability Distribution Models	AIC	BIC
Gumbel	317.606	280.773
Normal	435.689	398.862
Log Normal	402.744	368.341
Log Pearson type 3	321.502	284.870

In other research studies, similar findings have emerged. For instance, Bhat et al. (2019) conducted a flood frequency analysis on the Jhelum River in the Kashmir Basin and found that the Log Pearson Type-III distribution was a better fit than the Gumbel model when analyzing annual peak flow datasets. Likewise, Islam and Sarkar (2020) noted that Log Pearson Type 3 simulated discharges exhibited a closer approximation to a normal distribution compared to the Gumbel distribution, suggesting its greater reliability and suitability for flood forecasting in the Mayurakshi River Basin, India. Other studies that reported analogous results include Ewemoje and Ewemooje (2011) in the Ogun-Oshun River Basin, Nigeria, Farooq et al. (2018) in the River Swat, Pakistan, and Kumar (2019) in the Rapti River Basin.

Additionally, employing the maximum likelihood approach, Eris identified the Weibull function as the most appropriate probability distribution for analyzing eight sites in the Niger Basin. These research findings indicate that distribution functions may be suitable for estimating low, mean, and maximum flood frequencies at the same site. Therefore, the selection of an appropriate model for flood frequency analysis at a site with similar climatic, catchment, and hydrological characteristics depends on the frequency characteristics of the data series.

Consequently, the recommended distributions for the frequency characteristics in this basin were utilized to estimate flood events and their probabilities of occurrence. Using Gumbel's model for forecasting, it can be deduced that the probability of experiencing a flood magnitude falling within the range of 221.38 to 245 m³/s and 413.31 to 450 m³/s in the Gucha-Migori River Basin is 0.95 and 0.02, respectively. As a result, the model or mathematical equation derived from this analysis offers a satisfactory simulation of flood magnitudes and their corresponding annual exceedance probabilities.

4.2.7 Probability Distribution Curve for Gucha-Migori River Basin

Figure 4.18 presents the Probability Distribution Curve for Gucha-M River Basin.

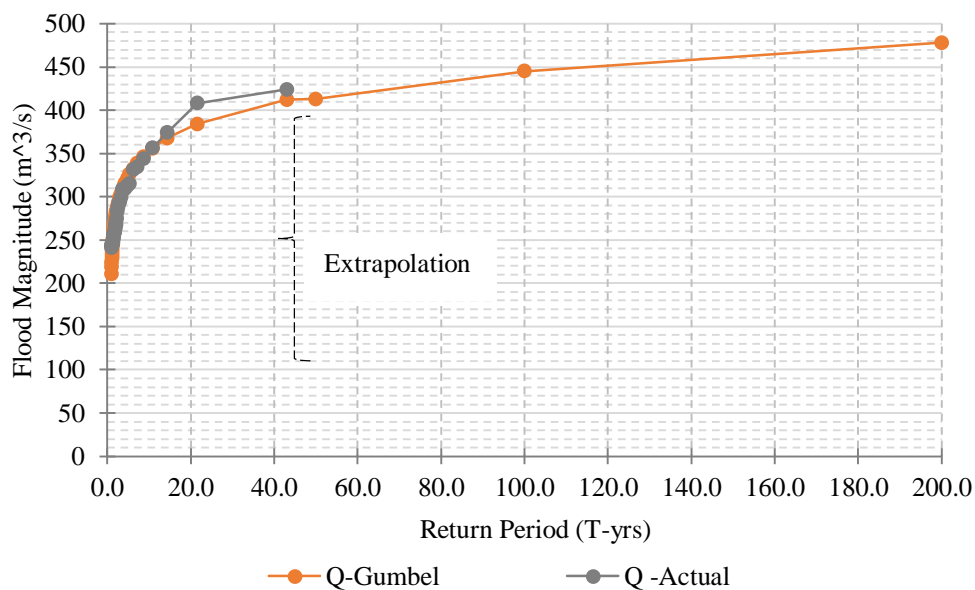


Figure 4.18: Probability Distribution Model for Gucha-Migori River Basin

According to the derived Gumbel's formula (Equation 4.1), the estimated flood magnitude for the return period 1.05, 1.11, 1.25, 2, 5, 10, 25, 50, 100, and 200 years were 221.38, 231.92, 245.77, 278.01, 321.39, 350.11, 386.39, 413.31, 440.03, and 466.65 m³/s correspondingly.

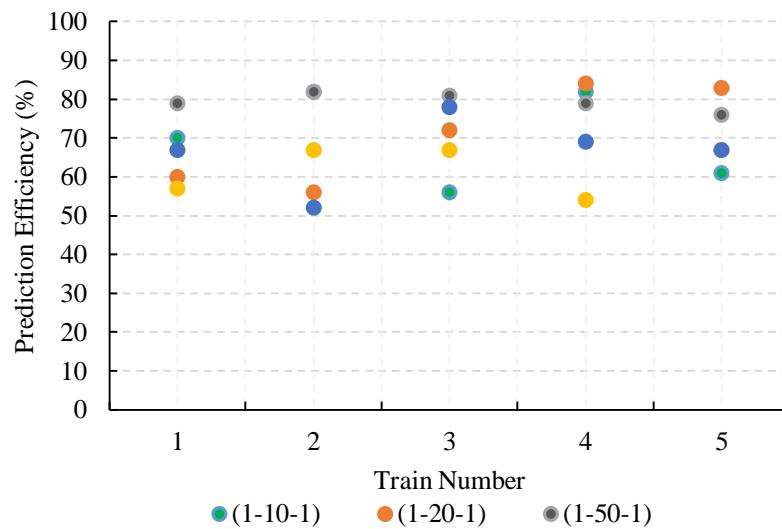
$$Magnitude(Q_T) = A(-\ln(-\ln(1 - \frac{1}{\lambda(T_{yrs})}))) + B \quad (4.1)$$

where; Q_T is the flood magnitude, A is equal to 38.279, T_{yrs} is the return period, λ is equal to 1, and B is equal to 263.99 m³/s.

4.3 Forecasting of the Flood Magnitude and Percent Annual Exceedance

4.3.1 Nonlinear Autoregressive Models Performance

Based on the results presented in Figure 4.19, the best prediction performance was achieved when the number of nodes in the hidden layer was 20. However, in all the trials, the efficiency was also relatively better when neurons in the hidden layer ranged from 20 to 50. From the analyses, it was revealed that the number of hidden layers and neurons per layer is completely flexible, and is optimized through an inbuilt algorithm of obtaining the network topology that provides the best performance (Ibnu Choldun et al., 2020). Nevertheless, increasing the number of neurons makes the system more complex, while a low number of neurons may restrict the generalization capabilities and computing power of ANN (Karsoliya, 2012; Stathakis, 2009; Uzair & Jamil, 2020).



1-10-1 is an architecture of the NAR model consisting of one input vector (historical datasets), and one hidden layer having 10 neurons to forecast a single output (future discharge).

Figure 4.19: Performance Efficiency of Various NAR Models

The performance of various nonlinear autoregressive neural network models in the forecasting of discharge is presented in Table 4.7. Considering all the trials, the highest and the lowest values of coefficient of correction ($R = (9.15e-1 \ \& \ 8.17e-1)$) and mean squared error ($MSE =$

(1613.54e-0 & 779.59e-0)) for testing, indicated a stronger correlation and that the models captured temporal discharge patterns at a very good level.

Using the comparative analysis, the network topology of 1-20-1 was adopted as the best NAR model for forecasting because of its minimum values of R for training (9.20e-1), validation (9.27e-1), and testing (9.15e-1). Its minimum values of MSE were as follows, for training (875.67e-0), validation (815.06e-0), and testing (779.59e-0). The R-values of the aforementioned NAR model indicated that the ANN of network topology (1-20-1) at trial 4 was capable of accounting for at least 84% of the variance of the input variable. It was the best model performance as per Moriasi et al.'s (2007) Van Liew et al.'s (2003), and Nastos et al.'s (2014) recommendations. Practical recommendations for future research and water resource management have been provided. These include specific areas for further investigation and actionable advice for policymakers to improve flood management and mitigation strategies.

Table 4.7: Nonlinear Autoregressive Models Performance

Network Architecture	Trial		Target Values	MSE	R
1-10 -1	T2	Training	1652	840.66e-0	9.18e-1
		Validation	206	998.83e-0	9.11e-1
		Testing	206	971.39e-0	9.09e-1
1-20-1	T4	Training	1652	875.67e-0	9.20e-1
		Validation	206	815.06e-0	9.27e-1
		Testing	206	779.59e-0	9.15e-1
1-50-1	T3	Training	1652	859.50e-0	9.21e-1
		Validation	206	773.16e-0	9.17e-1
		Testing	206	809.14e-0	9.01e-1
1-100-1	T5	Training	1652	769.37e-0	9.28e-1
		Validation	206	1216.57e-0	8.96e-1
		Testing	206	2027.06e-0	8.17e-1
1-200-1	T4	Training	1652	838.52e-0	9.25e-1
		Validation	206	1292.36e-0	8.83e-1
		Testing	206	1613.54e-0	8.83e-1

1-10-1 is an architecture showing that the NAR model consisted of one input vector (historical discharge data), and one hidden layer having 10 neurons to forecast a single output (discharge).

Other NAR models like 1-10-1, 1-50-1, 1-100-1, and 1-200-1 could only account for 82, 81, 67, and 69 % of the variance of the input vectors correspondingly. These results agree with findings from some studies such as Amisi (2021) and Le et al. (2020).

4.3.2 Best NAR Performance Indicators

As presented in Figure 4.20, the statistical indicators, the best validation performance for the NAR (1-20-1) adopted for forecasting was 815.0594 at epoch 9.

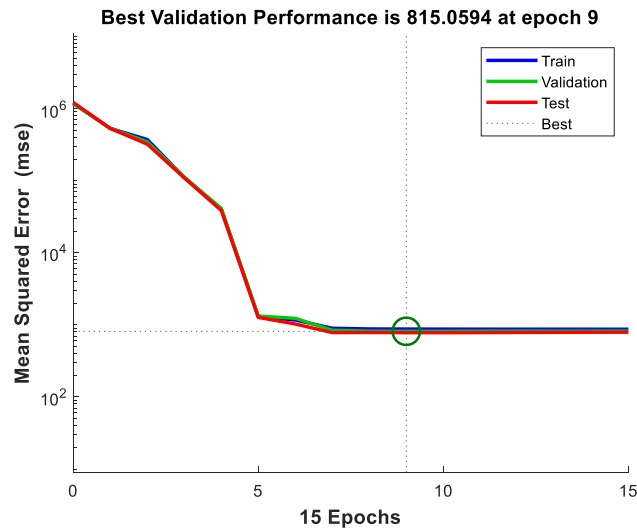


Figure 4.20: L-M algorithm MSE Output

Figure 4.21 shows the error between target values and predicted values after training the ANN model for the prediction of future discharge values for the G-M River Basin.

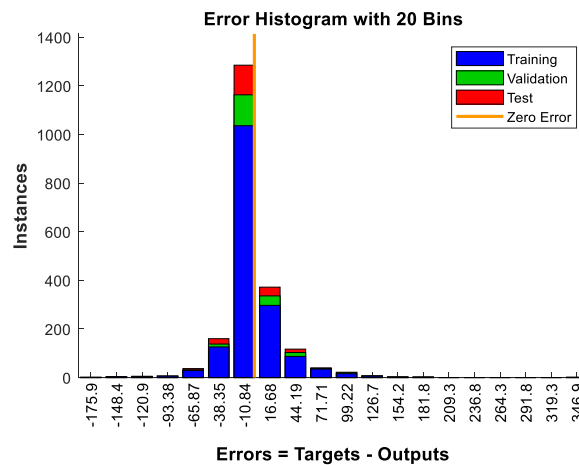


Figure 4.21: Error Histogram for the NAR Model

The number of vertical bars observed in this case was 20, hence, twenty smaller bins (Figure 4.21). In the middle of the plot, there is a bin corresponding to the error of -10.84 and the height of the bin for training datasets lies below but near 1100, and validation and test datasets lie between 1100 and 1300 indicating that many samples had an error lies in that following range. Nonetheless, these error values revealed a satisfactory performance.

Figure 4.22 represents the regression plots of the NAR model. The label of these graphs denotes an equation between the predicted value and the target value, with output as the dependent variable and target as the independent variable.

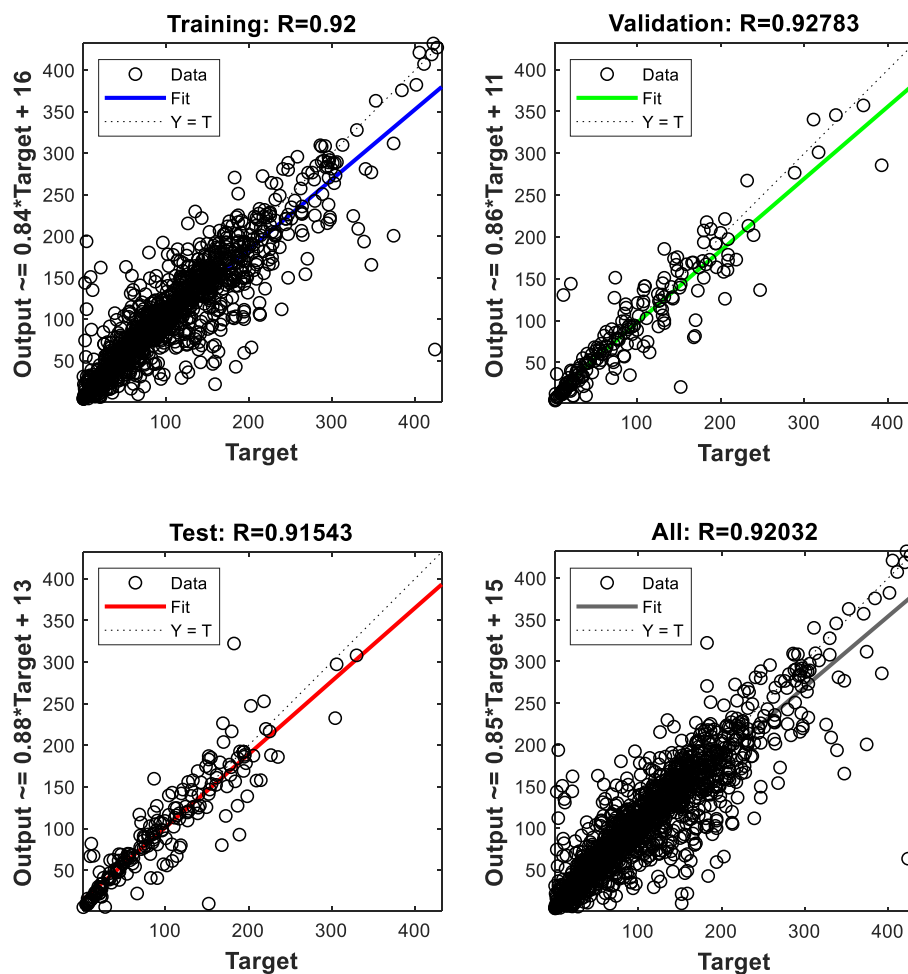


Figure 4.22: Regression of the best Nonlinear Autoregressive Neural Network

These equations clearly show that the nonlinear autoregressive model performance was highly acceptable and very good for forecasting discharge datasets. For example, it can be inferred that the correlation coefficient values for training, validation, and testing ($R = 0.92, 0.93,$ and

0.92), implied that the NAR model was capable of explaining at least 84 % of the variance of observed discharge datasets. The coefficient of the target shows the proportionality between the output and the targets (Karul et al., 2000; Sargent, 2001). Thus, for this scenario, the NAR was selected based on good performance criteria, which was evident that the correlation coefficient was close to a unit as possible, with the negligible disparity between the training and the testing accuracy.

Figure 4.23 shows the frequency-domain analysis for training, validation, and testing of 1-20-1 ANN to understand the stability and performance properties of the model adopted for forecasting.

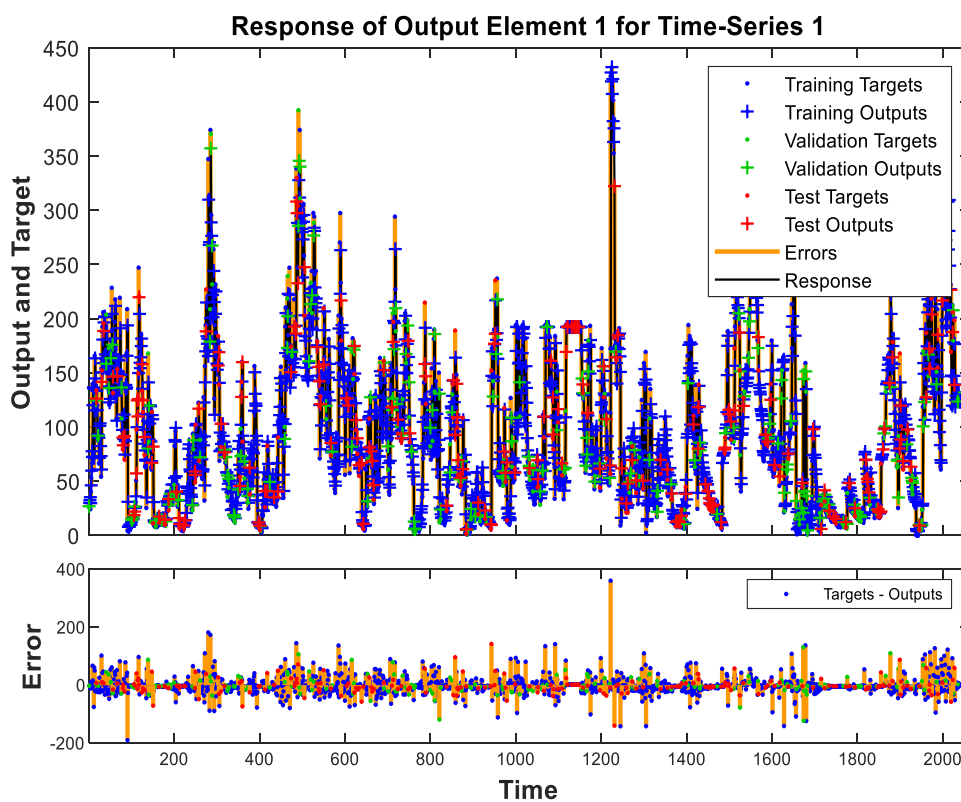


Figure 4.23: Time-Series Response of Nonlinear Autoregressive Neural Network

Validation and testing outputs of the nonlinear autoregressive neural networks showed a satisfactory response to peaks (flood magnitudes) related to extreme occurrences. The statistic indicators of the time series analysis (Figure 4.23) imply a NAR model with a high prediction accuracy and a relatively perfect linear covariation between observed and forecasted datasets. Other studies with similar modeling characteristics based on trained Artificial Neural Network models include Khan and Gupta (2020), Li and Chan (2017), and Wang et al. (2017).

Error autocorrelation is plotted in Figure 4.24. The results from the graph revealed the maximum correlations at zero lag.

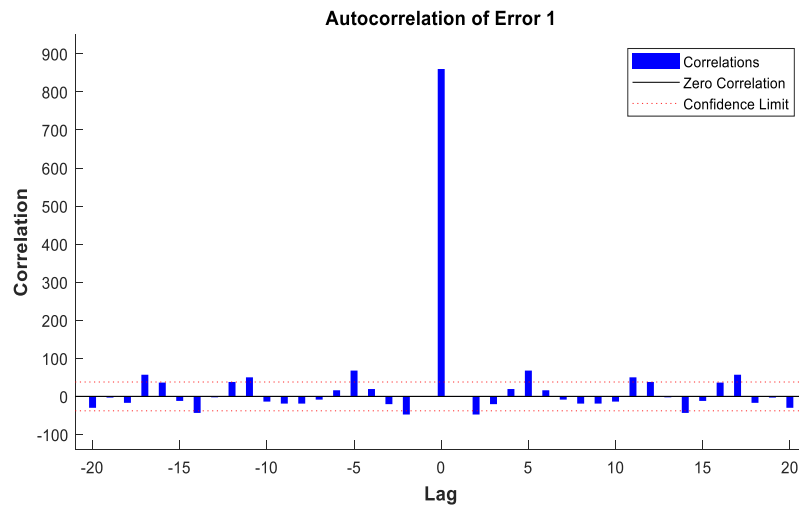


Figure 4.24: Error Autocorrelation of trained Nonlinear Autoregressive Neural Network

4.3.3 Time Series of Observed and Predicted Future Flood Events

Figure 4.25 shows a time series of observed and forecasted flood magnitudes with their respective annual non-exceedance probabilities.

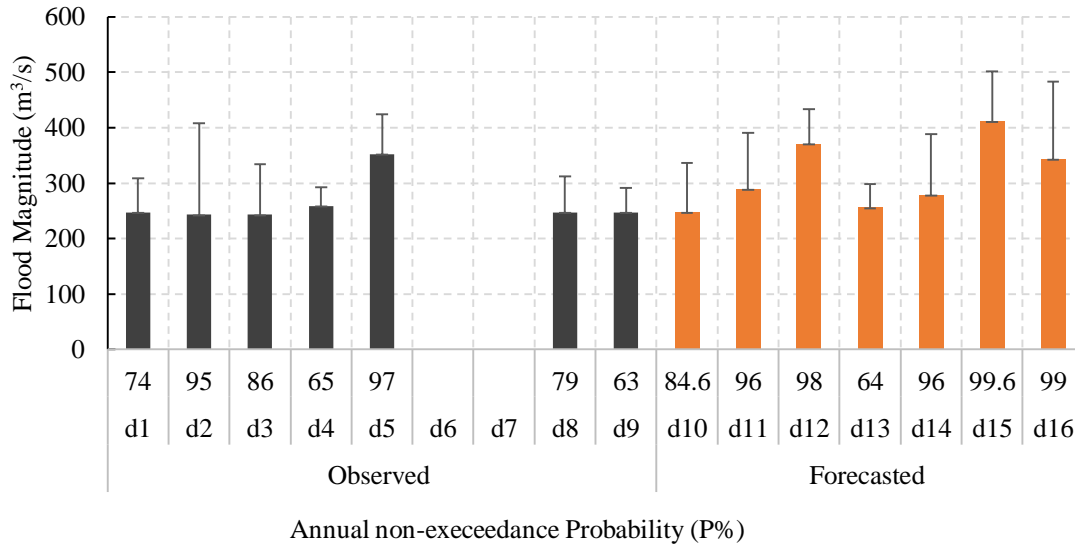


Figure 4.25: Forecasted Flood Magnitudes and their Frequencies

From the analysis, d1, d2, d3, d4, d5, d6, d7, d8, d9, d10, d11, d12, d13, d14, d15, and d16 represent (1969-1973), (1974-1969), (1979-1983), (1984-1988), (1989-1993), (1994-1998), (1999-2003), (2004-2008), (2009-2013), (2014-2018), (2019-2023), (2024-2028), (2029-2033), (2034-2038), (2039-2043), and (2048-2052) respectively. The findings show that the

daily river discharges and flood magnitudes will progressively increase in the periods 2022 and 2052. The positive trend was significant at $p < 0.01$ and the events may be described relatively perfectly by time as the independent variable (Figure 4.25). Daily river discharges positive trends in Gucha-Migori River Basin, will likely continue climatic scenarios following a polynomial curve of the third order.

Forecasted minimum flood magnitudes were 247, 289, 371, 256, 279, 412, and 343 m³/s for the periods (2014-2018), (2019-2023), (2024-2028), (2029-2033), (2034-2038), (2039-2043), and (2048-2052), respectively. In addition, the maximum forecasted flood magnitudes were 336, 391, 433, 299, 389, 502, and 483 m³/s for the periods 2014–2018, 2019–2023, 2024–2028, 2029–2033, 2034–2038, 2039–2043, and 2048–2052, respectively. Their respective annual non-exceedance probabilities from Gumbel's curve were 84.6, 96, 98, 64, 96, 99.6, and 99 % respectively. Forecasted flood magnitudes results agreed with flood studies within the catchments neighbouring Gucha-Migori River Basin such as Amisi (2021) as in Njoro, Githui et al. (2009) in Nzoia, Rwigi (2014) in Sondu, Mwangi et al. (2016) in upper Mara River, and Mbote (2016). The aforementioned studies' projections of an increase in water yield in future climatic scenarios are attributed to an increase in precipitation and surface air temperature.

CHAPTER FIVE

CONCLUSIONS AND RECOMMENDATIONS

5.1 Conclusions

This research successfully modelled and forecasted flood events in the Gucha-Migori River Basin, Kenya, providing valuable insights into flood dynamics and predictive capabilities. The following specific conclusions are drawn from the research findings:

(i) Model Performance and Predictive Accuracy:

The HEC-HMS model demonstrated moderate performance in simulating daily river discharge, with R^2 values of 0.52 during calibration and 0.42 during validation, and NSE values of 0.36 and 0.31 respectively. The significant positive correlation between daily precipitation and river discharge across different seasonal periods (JFM, AMJ, JAS, OND) indicates that precipitation is a critical driver of river discharge variability in the basin. These results highlight the need for further refinement of the model to improve predictive accuracy.

(ii) Flood Magnitude Estimation:

The Gumbel Probability Distribution was identified as the most suitable method for estimating extreme flood events in the Gucha-Migori River Basin. The derived Gumbel's formula provided reliable estimates of flood magnitudes for various return periods, ranging from 1.05 to 200 years. This method offers a robust tool for predicting flood magnitude, aiding in effective flood risk management and planning in the basin.

(iii) Flood Forecasting Using ANN:

The use of Artificial Neural Networks (ANN) combined with the Gumbel Probability Distribution achieved the best performance in forecasting flood magnitudes and their respective annual exceedance probabilities for the period between 2022 and 2052. The optimal configuration was found with 20 nodes in the hidden layer. This approach demonstrates the potential of integrating machine learning techniques with traditional hydrological models to enhance flood forecasting accuracy and reliability.

5.2 Recommendations

Practical recommendations for future research and water resource management have been provided. These include specific areas for further investigation and actionable advice for policymakers to improve flood management and mitigation strategies:

(i) Utilization of the HEC-HMS Model with Reliable Data:

The HEC-HMS model should be employed with reliable data from multiple meteorological stations to better understand the spatial-temporal effects of precipitation variability on river discharge. This approach may help reduce errors and uncertainties during the modeling set-up, parameterization, calibration, and validation processes.

(ii) Adoption of the Gumbel Probability Distribution Model:

Based on the data products from this analysis, the study recommends the adoption of the Gumbel probability distribution model for analyzing extreme events, specifically for flood forecasting in the Gucha-Migori River Basin. This model can provide a more accurate representation of the frequency and magnitude of extreme flood events.

(iii) Hydrological Forecasting with Advanced Techniques:

Future research should explore hydrological forecasting by integrating various types of Artificial Neural Networks (ANNs) and Probability Distribution Models to predict hydrologic variables under different future scenarios. This technique should also be tested in other catchments to validate its effectiveness. Furthermore, the use of artificial intelligence (AI) and machine learning (ML) techniques should be expanded to enhance predictive accuracy and reliability.

These recommendations aim to improve the understanding and management of flood risks, leveraging advanced modeling techniques and robust data analysis.

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APPENDICES

Appendix A: Tables

Table 1A: Attributes of the downloaded Landsat 1-3 Satellite Data

	Band	Wavelength	Spatial Resolution
		Spectral Range (μm)	(m)
Landsat 1-3	Band 4 - Green	0.5-0.6	60
	Band 5 - Red	0.6-0.7	60
	Band 6 – Near IR	0.7-0.8	60
	Band 7 – Near IR	0.8-1.1	60

Table 2A: Attributes of the downloaded Landsat 4-5 Satellite Data

	Band	Wavelength	Spatial Resolution
		Spectral Range (μm)	(m)
Landsat 4-5	Band 1 – Blue	0.45-0.52	30
	Band 2 – Green	0.52-0.60	30
	Band 3 – Red	0.63-0.69	30
	Band 4 – Near IR	0.77-0.90	30
	Band 5 – Short -wave IR	1.55-1.75	30
	Band 6 – Thermal IR	10.40-12.50	120
	Band 7– Shortwave IR	2.09-2.35	30

Table 3A: Attributes of the downloaded Landsat 7 Satellite Data

	Band	Wavelength	Spatial Resolution
		Spectral Range (μm)	(m)
Landsat 7	Band 1 – Blue	0.45-0.52	30
	Band 2 – Green	0.52-0.60	30
	Band 3 – Red	0.63-0.69	30
	Band 4 – Near IR	0.77-0.90	30
	Band 5– Short wave IR1	1.55-1.75	30
	Band 6 – Thermal IR	10.40-12.50	30/60
	Band 7– Shortwave IR2	2.09-2.35	30
	Band 8- Pan	0.52-0.90	15

Table 4A: GPS points used for Geo-referencing in image classification

Latitude	Longitude	Description	Classified LULC
-0.9186886	34.1629787	Kabuto area	Farm land
-0.9324261	34.1706723	Relocated to new position due to flood	Kabuki Primary school
-0.9200208	34.1671365	River Gucha Migori river banks	Sand Harvesting
-0.9329420	34.1723661	Kabuto Area	Residential area
-0.9959811	34.2261873	Ogoche area	Farm lands
-0.9967397	34.2276904		Bare land with minimal activity
-0.9224677	34.2126381	Nyatike area	Nyatike irrigation scheme
-0.9268485	34.2274315	Gunga stream	Rice farming

Table 5A: GPS points used for Geo-referencing of stream digitization

Latitude	Longitude	Description
-0.9194701	34.1656569	River Gucha-Migori
-0.9298539	34.1783116	River Dike, used to prevent flood water from crossing over to the residential areas
-0.9401968	34.1825582	Original River Gucha-Migori route, changed in 2003
-0.9965885	34.2273561	Ogoche Stream, seasonal river on the upstream
-0.9500831	34.2101668	1KB 05 gauging station
-0.8985250	34.1924344	Obware Stream
-0.9884325	34.24976	Gucha- Migori Sango, where the two rivers meet
-0.9709883	34.260812	River Kuja
-0.9925320	34.2918827	River Migori

Appendix B: Figures

Each figure in the Results and Discussion chapter is accompanied by a detailed explanation, describing what the figure shows, interpreting the data, and explaining its relevance to the study. Figures are well-labeled and referenced in the text.

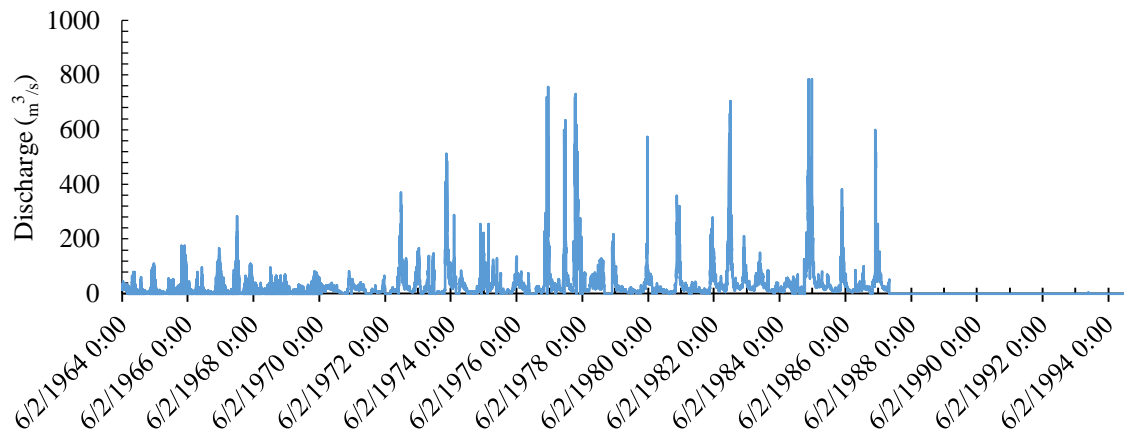


Figure 1B: 1KB01A-Gucha Macalder [m³/s] (Position: 34.2732, -0.9548 Decimal Degrees)

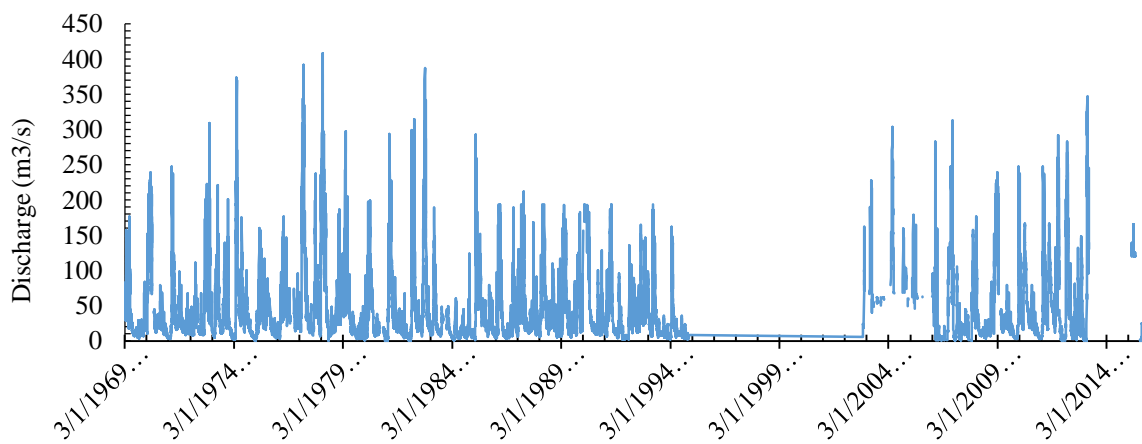


Figure 2B: 1KB05-Gucha Migori [m³/s] (Position: 34.2096, -0.9492 Decimal Degrees)

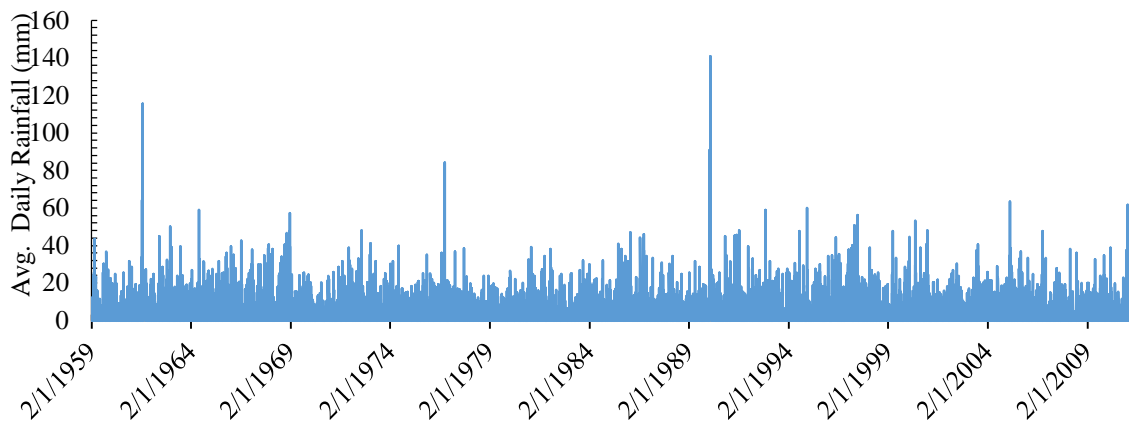


Figure 3B: Gucha-Migori River Basin Average Daily Rainfall (mm)

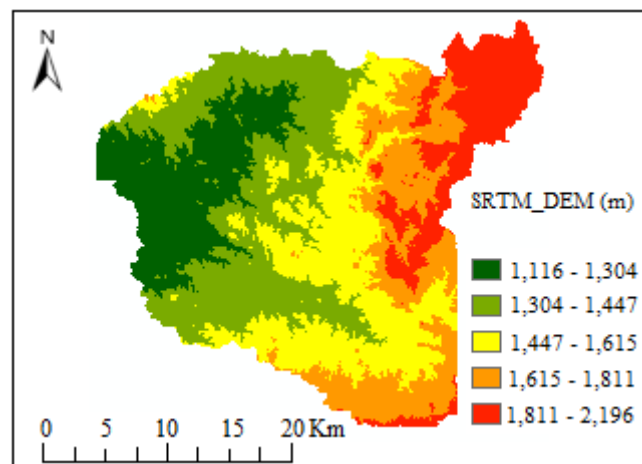


Figure 4B: Shuttle Radar Topography Mission-DEM for Gucha-Migori River Basin

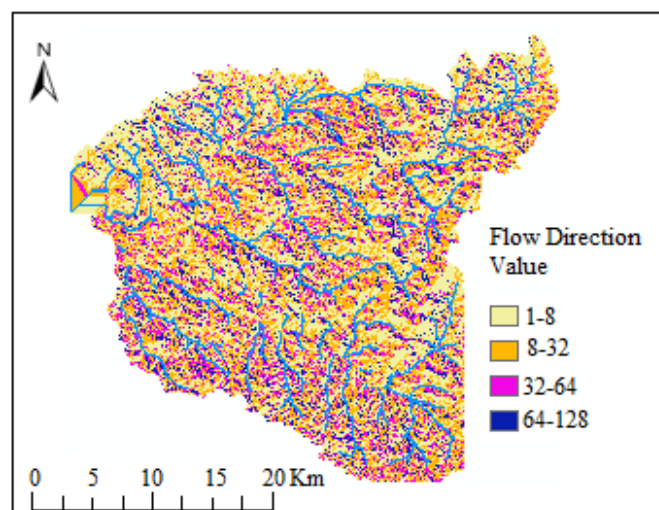


Figure 5B: Flow Direction Processing using GeoHMS and Arc Hydro tools

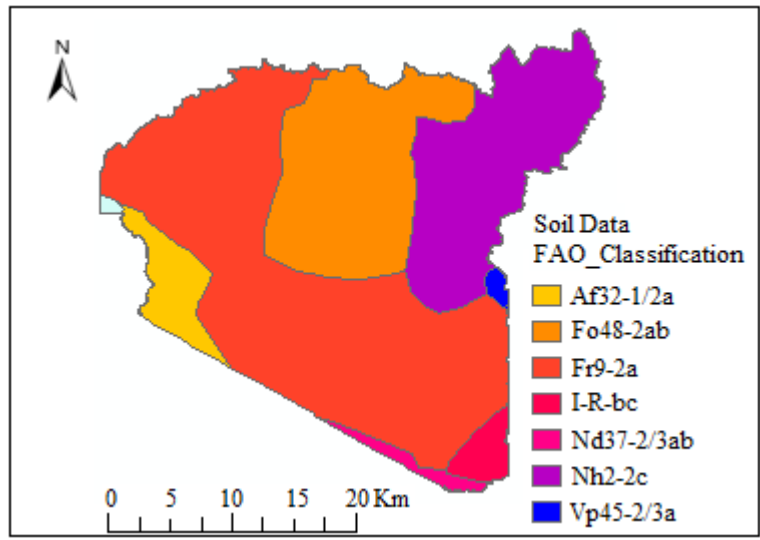


Figure 6B: FAO soil classification at Gucha-Migori River Basin

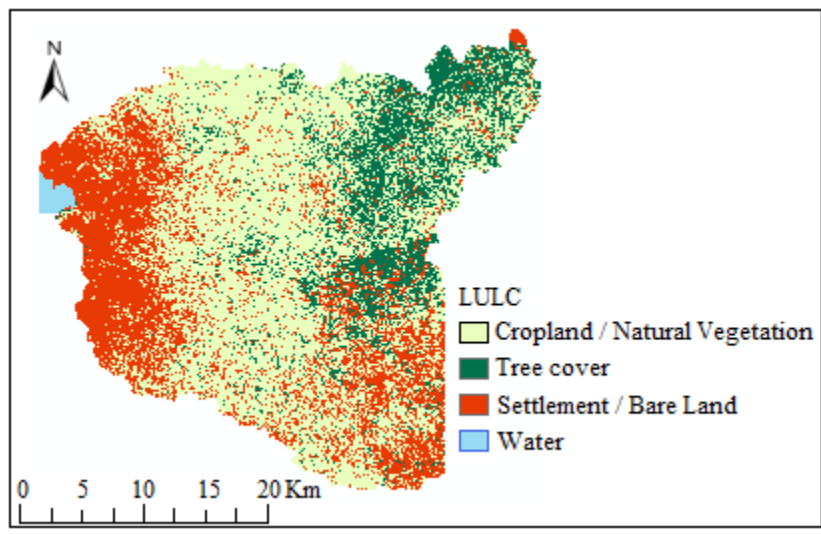


Figure 7B: Classified Landsat MSS image of 1976 for Gucha-Migori River Basin

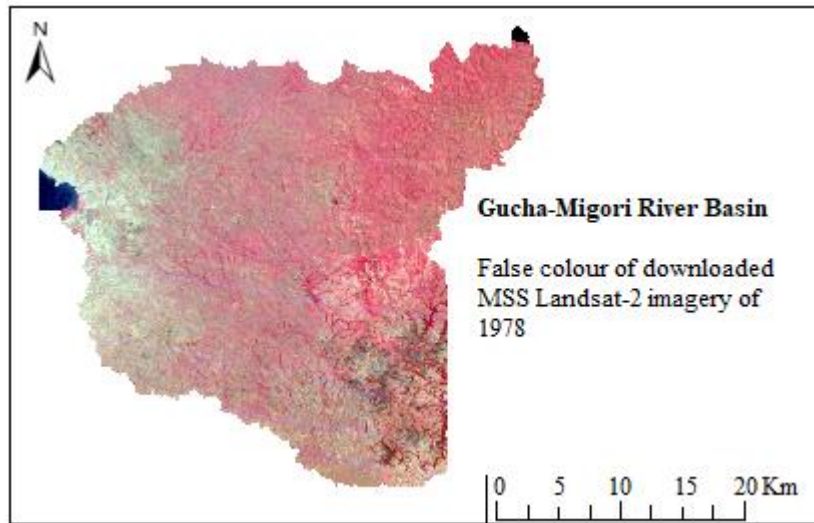


Figure 8B: Shows an imagery for raster MTL.text 4Bands (Green, Red, Near Infrared 1, and Infrared 2) for Gucha-Migori River Basin

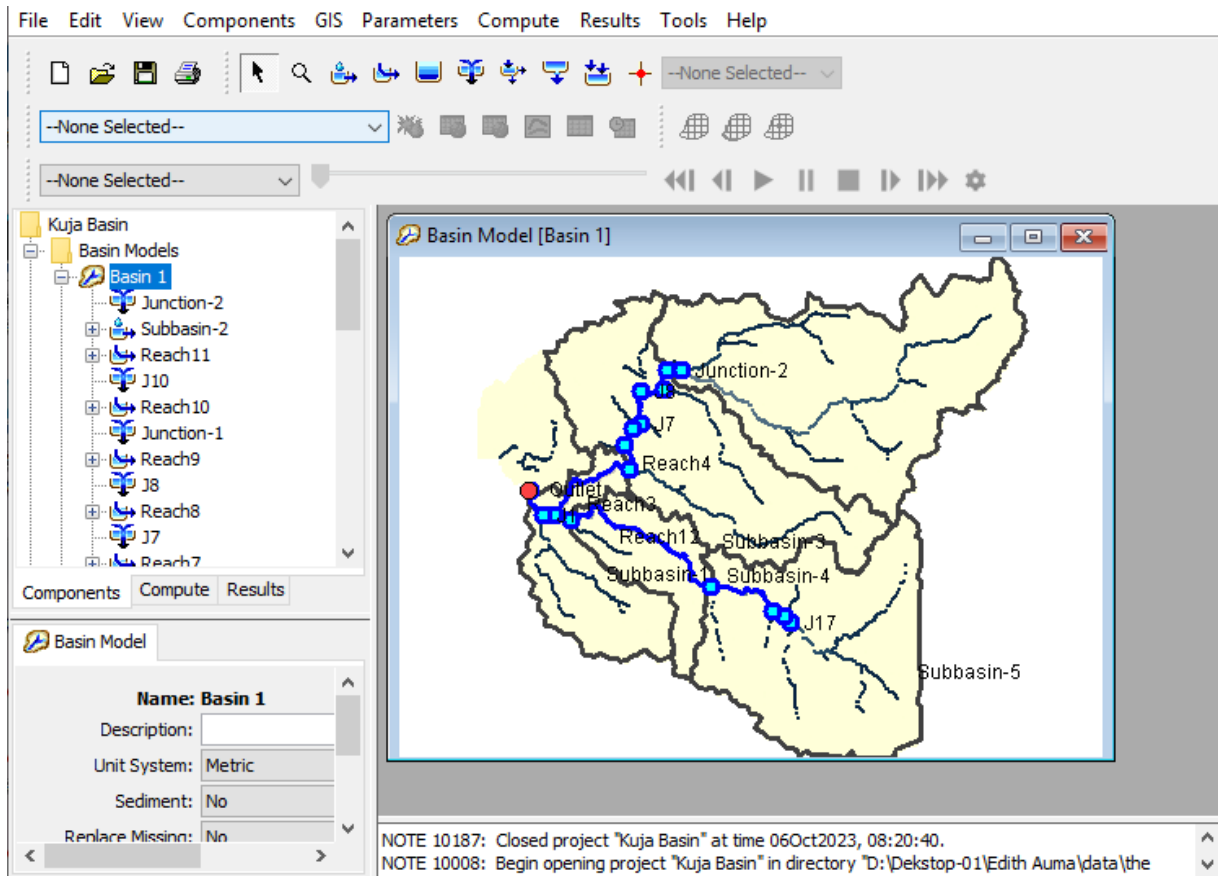


Figure 9B: The HEC-HMS Modelling Process for Gucha-Migori River Basin

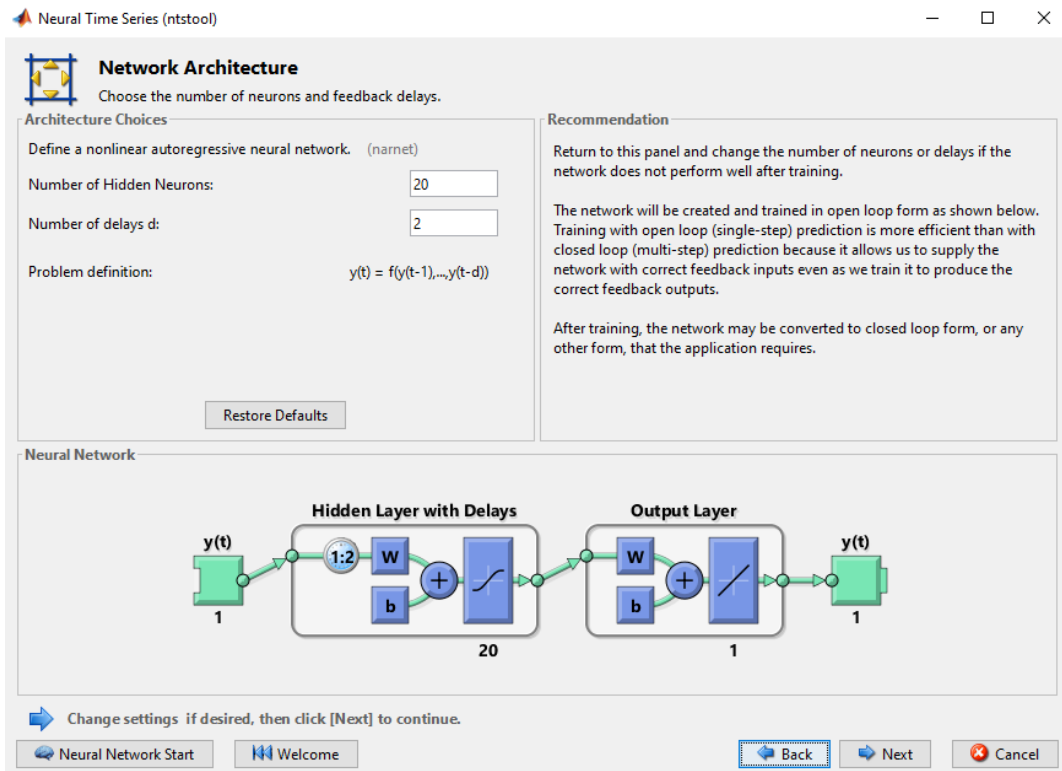


Figure 10B: Selection of the number of neurons and feedback delays

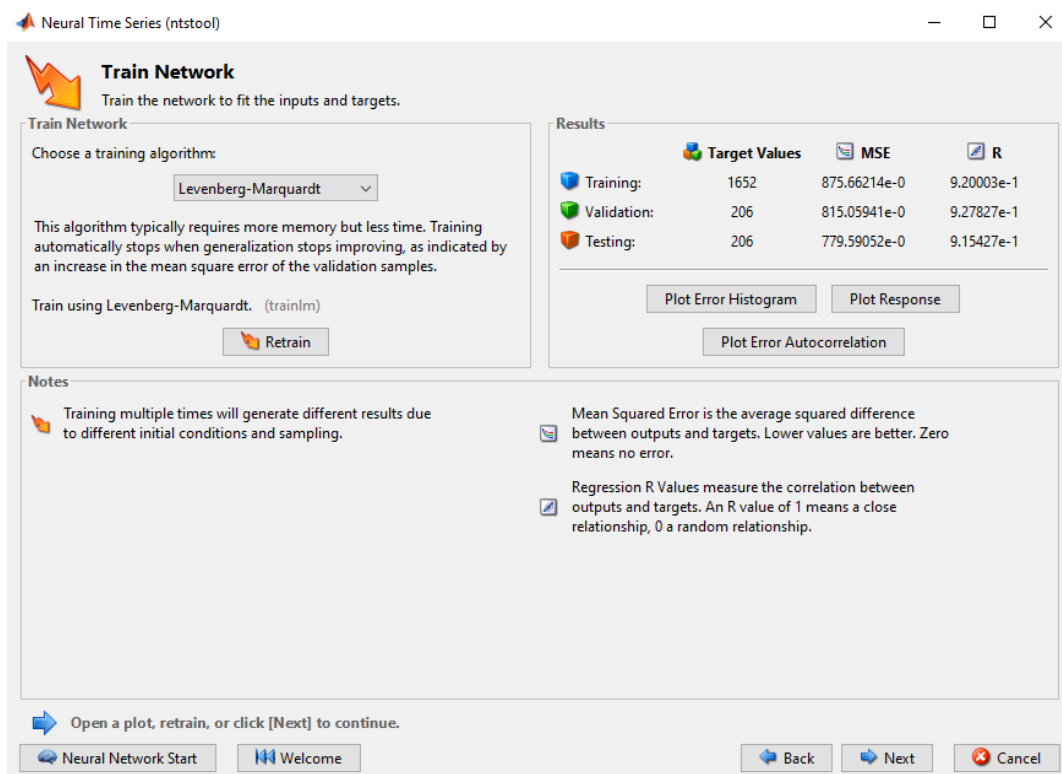


Figure 11B: Training the network to fit the inputs and targets in MATLAB

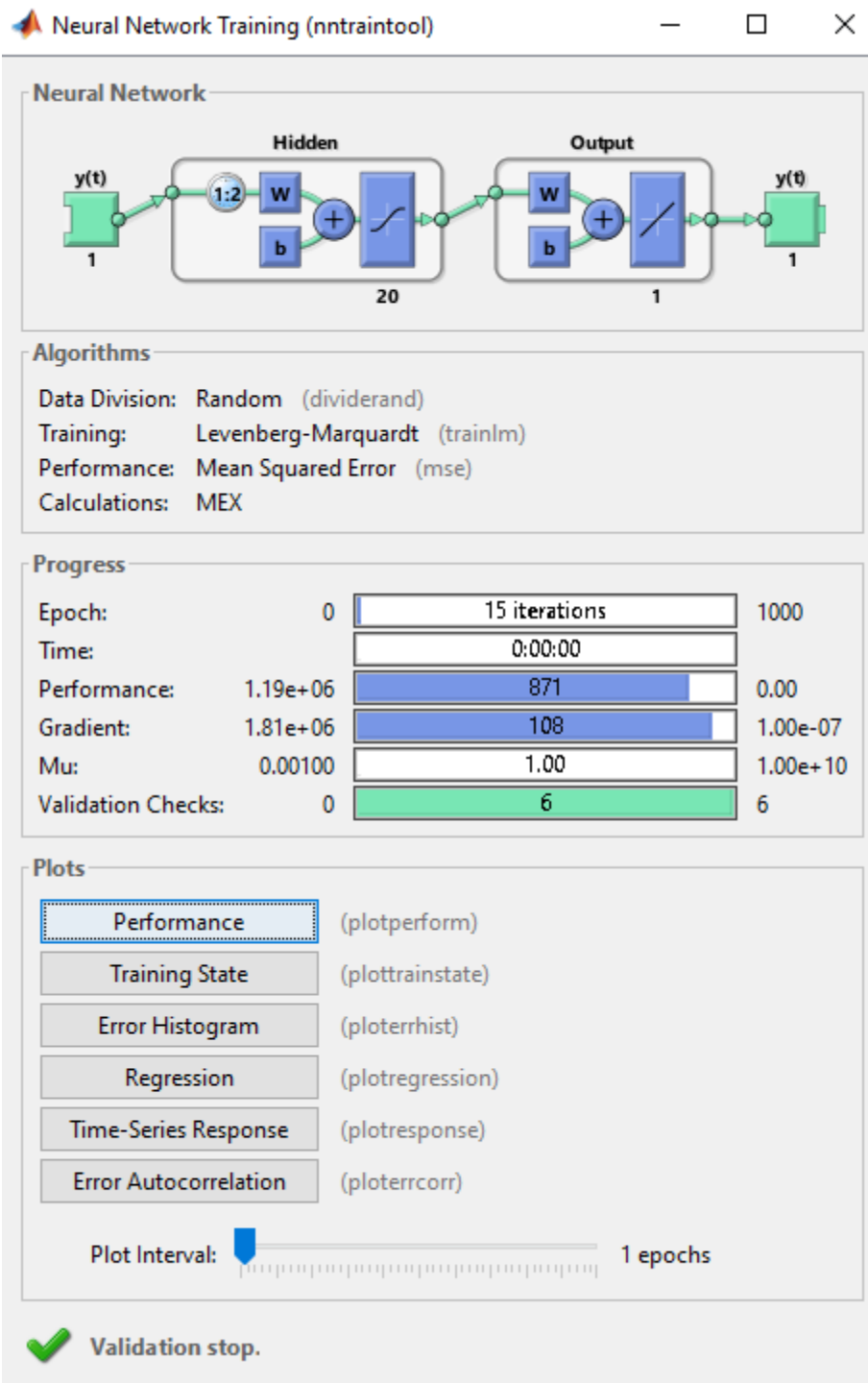


Figure 12B: ANNs Performance, Training State, and Time Series Response



Figure 13B: IKB05 River Gauging Station & Ogoche Stream



Figure 14B: Sand harvesting along the River Kuja Banks



Figure 15B: River Kuja at Obware Stream








Figure 16B: Nyatike Irrigation Scheme



Figure 17B: Gucha Migori Sango, Confluence of the two rivers

Appendix C: Research License

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FORECASTING OF FLOOD EVENTS FOR WATER RESOURCES MANAGEMENT IN GUCHA-MIGORI RIVER BASIN, KENYA

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ABSTRACT

Floods are devastating natural disasters frequently occurring in many river basins such as Gucha-Migori River Basin, Kenya. However, non-structural countermeasures such as hydrologic modelling, flood proofing, and continuous forecasting have not been fully explored and implemented to reduce risk, damage, and vulnerabilities of flood events. The major challenge in flood forecasting is the selection of the relevant probability distribution. The main objective of the study was to forecast flood events in Gucha-Migori River Basin for integrated water resource management. Daily hydrological datasets between 1969 and 2015 were obtained from Water Resources Authority. After the ranking of independent flood events had been achieved, return periods and flood frequencies were computed. The relationship between flood magnitudes and their respective frequencies was through modelling using probability distribution functions (PDFs). The evaluated PDFs include Normal Distribution, Log-Normal Distribution, Gumbel Distribution, and Log-Person Type III Distribution. Coefficient of Determination (R^2), Goodness of Fit test, and Best-Fit Distribution Curve guided selection of the suitable distribution model. The suitable probability distribution model out of the tested four was then applied to predict P-percent annual exceedance probabilities corresponding to specific flood magnitudes. From the results, out of the 132 flood events that occurred in the period 1969 to 2015, only 42 were identified as independent flood events. Based on the frequency analysis, the highest and lowest, and the average and standard deviation of the recorded independent flood events were 423.90, 240.8, 284.80 m³/s, and 45.54 respectively. It was revealed that the probability of a flood event of a magnitude equal to or exceeding the lowest (240.8 m³/s) and the highest (423.90 m³/s) occurring for a particular year were 0.98 and 0.02 respectively. Gumbel distribution curve was selected to be the best fit for the Gucha-Migori River Basin. According to the derived Gumbel's formula, the estimated magnitude for the return period 1.05, 1.11, 1.25, 2, 5, 10, 25, 50, 100, and 200 years were 221.38, 231.92, 245.77, 278.01, 321.39, 350.11, 386.39, 413.31, 440.03, and 466.65 m³/s. This research provides useful information for enhanced determination of probability occurrence of flood events and thus proper water resources planning and management strategies in the Gucha-Migori river basin.

Keywords: Flood Discharge, Probability Distribution Models, Forecasting, Flood Frequency

1.0. INTRODUCTION

Climate change and growing socio-economic developments continue to alter hydrological regimes and the response of several watersheds

globally, thus threatening water, energy, and food security (Archer et al., 2010; IPCC, 2014; UNFCCC, 2005; Wambua et al., 2017). In Kenya, there is a study recognition of ecosystem deterioration, and spatio-temporal uncertainties